







**TPS272C45**

ZHCSM06B – DECEMBER 2020 – REVISED FEBRUARY 2022

# **TPS272C45 45MΩ** 双通道智能高侧开关,带诊断功能

# **1** 特性

**TEXAS** 

**INSTRUMENTS** 

- 适用于 24V 工业应用的低 R<sub>DS(on)</sub> (典型值 45mΩ)高侧开关
- 宽直流工作电压范围:6V 至 36V
- 24V 电源供电时具有低静态电流 (Iq):0.5mA/通道 (典型值)
- 固定 (5.8A) 及可调节(可通过外部电阻器调节为 0.7A 至 4A)电流限制
- 可驱动电感、容性和电阻性负载
	- 集成输出钳位支持电感负载放电
	- 容性负载驱动可通过双重阈值电流限制功能尽可 能降低浪涌电流峰值
- 强大的输出保护
	- 热关断
	- 接地短路保护
	- 可配置故障处理
- 增强型诊断特性
	- 输出负载电流测量
	- 开路负载(关闭状态)检测
- 封装: 24 引脚 QFN (5mm × 4mm)
- 提供功能安全
	- 有助于进行功能安全系统设计的文档

# **2** 应用

- 工业 PLC 系统
	- 数字输出模块
	- IO-Link 主站端口
- 电机驱动器
- 楼宇自动化系统

# **3** 说明

TPS272C45 是一款旨在满足工业控制系统要求的双通 道智能高侧开关。低导通电阻 (R<sub>DS(on)</sub> 为 45mΩ ) 可 最大限度地降低器件功耗,实现 100mA 至 3A 的宽输 出负载电流范围。该器件提供一个额外的低压电源 (3.3V 至 5V)输入引脚,从而最大限度地降低空载功 耗。该器件集成了多种保护功能,如热关断、输出钳位 和过流限制。这些功能可在发生故障(如短路)时提高 系统的稳健性。

TPS272C45 器件采用可调阈值电流限制电路,通过减 小驱动大容性负载时的浪涌电流并尽可能降低过载电 流,提高了系统的可靠性。该器件还可配置浪涌电流持 续时间,可通过较高的电流驱动高浪涌电流负载(如 灯)或快速为容性负载充电。该器件还可提供精确的负 载电流感测,以提高负载诊断功能,从而更好地进行预 测性维护。

TPS272C45 器件采用引脚间距为 0.5mm 的 24 引脚 5mm × 4mm 小型 QFN 无引线封装,从而最大限度地 减小 PCB 尺寸。

器件信息

器件型号	-------- 封装(1)	均装尺寸 (标称值)
TPS272C45	'QFN (24)	15.00mm × 4.00mm

(1) 如需了解所有可用封装,请参阅数据表末尾的可订购产品附 录。







# **Table of Contents**





# **4 Revision History**

注:以前版本的页码可能与当前版本的页码不同





# **5 Device Comparison Table**





# **6 Pin Configuration and Functions**



表 **6-1. Pin Functions**



**TEXAS INSTRUMENTS www.ti.com.cn**



# 表 **6-1. Pin Functions (continued)**



# **6.1 Recommended Connections for Unused Pins**

The TPS272C45 is designed to provide an enhanced set of diagnostic and protection features. However, if the system design only allows for a limited number of I/O connections, some pins can be considered as optional.



# 表 **6-2. Connections for Optional Pins**



# **7 Specifications**

#### **7.1 Absolute Maximum Ratings**

Over operating free-air temperature range (unless otherwise noted) $(1)$ 



(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute maximum rated conditions for extended periods may affect device reliability.

# **7.2 ESD Ratings**



(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

(3) Tested with application circuit and supply voltage (VS) of 24-V, ENx pins High (Output Enabled) and and EN pins Low (Outputs Disabled)

# **7.3 Recommended Operating Conditions**

over operating free-air temperature range (unless otherwise noted) (1)



# **7.3 Recommended Operating Conditions (continued)**

over operating free-air temperature range (unless otherwise noted) (1)



(1) All operating voltage conditions are measured with respect to device GND

# **7.4 Thermal Information**



(1) For more information about traditional and new thermal metrics, see the SPRA953 application report.

(2) The thermal parameters are based on a 4-layer PCB according to the JESD51-5 and JESD51-7 standards.

# **7.5 Electrical Characteristics**















V<sub>S</sub> = 6 V to 36 V, V<sub>DD</sub> = 3.0 V to 3.6 V, T<sub>J</sub> = -40°C to 125°C (unless otherwise noted)



(1) The maximum current output under overload condition before current limiting occurs.

(2) SEL must be set to select the relevant channel. Diagnostics are performed on Channel 1 when SEL = 0 and diagnostics are performed on channel 2 when SEL =1

# **7.6 SNS Timing Characteristics**

V<sub>S</sub> = 6 V to 36 V, T $_{\textrm{\scriptsize{J}}}$  = -40°C to +125°C (unless otherwise noted)



# **7.7 Switching Characteristics**

V<sub>S</sub> = 6 V to 36 V, T $_{\textrm{\scriptsize{J}}}$  = -40°C to +125°C (unless otherwise noted)





# **7.7 Switching Characteristics (continued)**

V<sub>S</sub> = 6 V to 36 V, T $_{\textrm{\scriptsize{J}}}$  = -40°C to +125°C (unless otherwise noted)





# **7.8 Typical Characteristics**











# **8 Parameter Measurement Information**



图 **8-1. Parameter Definitions**



A. Rise and fall time of  $V_{EN}$  is 100 ns.







Rise and fall times of control signals are 100 ns. Control signals include: EN, DIA\_EN, SEL SEL pin must be set to the appropriate value.

# 图 **8-3. SNS Timing Characteristics Definitions**



# **9 Detailed Description**

# **9.1 Overview**

The TPS272C45 device is a dual channel 45-m Ω smart high-side switch that is intended to provide protection for output ports in 24-V Industrial systems. The device is designed to drive a variety of resistive, inductive and capacitive loads. The device integrates various protection features including overload protection through current limiting, thermal protection, and short-circuit protection. For more details on the protection features, refer to the *Feature Description* and *Application Information* sections of the document.

In addition, the device diagnostics features include the analog SNS output that is capable of providing a signal proportional to the load current flowing through the switch or constant high current as a fault indication. The highaccuracy load current sense allows for integration of load diagnostic features that can enable predictive maintenance for the system by watching for leading indicators of load failures. The device also integrates open load detection to enable protection against wire breaks. In addition, the device includes a single open drain FLT pin output (version A, B, C) and dual FLT pin outputs (version D) that indicate device fault states such as short to GND, short to supply, or overtemperature.

The TPS272C45 is one device in TI's industrial high side switch family. For each device, the part number indicates elements of the device behavior.  $\mathbb{F}\left[\mathbb{R}\right]$  explains the device nomenclature.



图 **9-1. Naming Convention**



# **9.2 Functional Block Diagram**



# **9.3 Feature Description**

# **9.3.1 Programmable Current Limit**

The TPS272C45 integrates a dual stage adjustable current limit. For the most efficient and reliable output protection, the current limit can be set as close to the DC current level as possible. Sometimes, systems require high inrush current handling as well (example incandescent lamp and capacitive loads). By integrating a dual stage current limit, the TPS272C45 enables robust DC current limiting while still allowing flexible inrush handling.

With the adjustable current limit feature, a lower current limit setting can reduce the fault energy and the output current during a load failure event such as a short-circuit or a partial load short (soft-short). By lowering fault energy and current, the overall system improves through:

- Reduced size and cost in current carrying components such as PCB traces and module connectors
- Less disturbance at the power supply (VS pin) during a short circuit event
- Less additional budget for the power supply to account for overload currents in one channel or more
- Improved protection of the downstream load



#### *9.3.1.1 Inrush Current Handling*

The TPS272C45 uses a resistor from the following pins to the IC GND to configure the current limit behavior: ILIM1, ILIM2, and ILIMD. The ILIM1 and ILIM2 pin resistors set the current limit thresholds for CH1 and CH2 respectively while ILIMD pin resistor sets a delay time for the device to operate in a higher or lower current limit during device start-up or output turn-on by retry after a fault (thermal) shutdown).



图 **9-2. Current Limit Set Functionality**

The ILIM1/ILIM2 thresholds and the ILIMD pin resistor controlled timing enable flexible inrush current control behavior. The following table shows the various options available.



#### 表 **9-1. Inrush Current Limit Options**

#### 表 **9-2. Delay Resistor Values**







图 **9-3. Inrush Current Control (Case 2) With a Shorted Load**



图 **9-4. Inrush Current Control (Case 3) With a Shorted Load**

For the Case 2, when the ENx pin goes high to turn on one of the channels (or the channel is turned on automatically to retry after a fault shutdwon), the device defaults to twice current limit threshold as determined by  $R_{I L I M1}/R_{I L I M2}$  or the maximum internal current limit level (whichever is lower). The internal current limit level is defined in the *Specifications* section of this document. After a T<sub>DELAY</sub> period that is determined by R<sub>ILIMD</sub>, the current limit changes to the threshold determined by  $R_{ILM1}/R_{ILM2}$ . The delay can be set in the range from 0 (the current limit threshold at all times set to that determined by  $R_{\vert L \vert M1}/R_{\vert L \vert M2}$  to a maximum of 22 ms in dscrete steps.



Each channel operates independently with current limit thresholds controlled by  $R_{I L I M1}$  and  $R_{I L I M2}$ (so both channels can have separate current limit thresholds). If channel 2 is enabled after channel one, channel 2 has its own separate timing.

The initial inrush current period when the current limit is higher enables two different system advantages when driving loads

- Enables higher load current to be supported for a period of time of the order of milliseconds to drive high inrush current loads like incandescent bulb loads.
- Enables fast capacitive load charging. In some situations, it is ideal to charge capacitive loads at a higher current than the DC current to ensure quick supply bring up. This architecture allows a module to quickly charge a capacitive load using the initial higher inrush current limit and then use a lower current limit to reliably protect the module under overload or short circuit conditions.

While in current limiting mode, at any level, the device has a high power dissipation. If the FET temperature exceeds the over-temperature shutdown threshold, the device turns off just the channel that is overloaded. After cooling down, the device either latches off or re-tries, depending on the state of the LATCH pin. If the device is turning off prematurely on start-up, TI recommends to improve the PCB thermal layout, lower the current limit to lower power dissipation, or decrease the inrush current (capacitive loading).

# *9.3.1.2 Calculating RILIMx*

To set the current limit thresholds, connect resistors from both ILIM1 and ILIM2 pins to GND. The current limit threshold for each channel is determined by Equation 1 (R<sub>ILIMx</sub> in k Ω):

$$
I_{CL} = K_{CL} / R_{ILIMx}
$$
 (1)

The nominal K<sub>CL</sub> value to be used in the calculation is 20.5 A.k Ω. The allowed R<sub>ILIMx</sub> range is between 5 k Ω and 28.2 kΩ. If either pin is floating, grounded, or outside of the range specified, the current limit defaults to an internal level that is defined in the *Specifications* section of this document.

# *9.3.1.3 Configuring ILIMx From an MCU*

In many situations, modules like to allow the current limit to be set programmatically from an MCU. This action enables a module to set current limits to fit the load after determining what load is plugged in. As described, the TPS272C45 current limits are set by  $R_{\text{lLIMx}}$ . However, the  $R_{\text{lLIMx}}$  that is seen by the device can be configured through small external FETs as shown in  $\overline{\otimes}$  9-5.



图 **9-5. Dynamic ILIMx Control**

For example, R<sub>ILIM1</sub> 1 can set the device to 500-mA ILIM while R<sub>ILIM1</sub> 2 can set the device at 2-A ILIM. After the MCU realizes how much current draw is required by the load, the MCU can drive one of the series FET's to set



the ILIM to be ideal for the specific load. The current limit (ILIM1 and ILIM2) thresholds can be changed dynamically, but the inrush current limit delay set with the ILIMD resistor cannot be changed after powerup.

The external FET switches used to dynamically adjust the current limit must be chosen with a minimum capacitance (Coss) from the drain the ground. The total capacitance to PCB ground at the ILMx pins including from traces must be limited to less than 100 pF.

#### **9.3.2 Low Power Dissipation**

There are two primary sources of power dissipation in the TPS272C45:

- 1. Resistive losses in the primary FET, which are calculated as  $(l_{\mathsf{LOAD}})^2 \times \mathsf{R_{ON}}$
- 2. Controller losses due to quiescent operating current, which are calculated as  $I_0 \times V_{\text{SUPPI}Y}$

If  $I_{\text{LOD}}$  is significantly more than 1 A, the resistive losses dominates the controller losses and they can be ignored. However, if  $I_{\text{LOAD}}$  is less than 1 A, the controller losses comprise a significant portion of the total device power dissipation. To lower the controller losses, version A of the TPS272C45 introduces a secondary low voltage supply on pin VDD that can power much of the device functionality. By lowering the controller supply voltage from 24 V to 3.3 V, the total controller losses decrease significantly.  $\frac{1}{\sqrt{6}}$  9-3 shows the impact this second supply can make on the total device power dissipation calculated at a worst case supply voltage of 30 V, without diagnostics enabled. There is an additional contribution to power dissipation from the current sense circuitry as well as the sensed current out of the SNS pin when diagnostics are enabled. Savings of over 80 mW per channel in the IC is achieved by powering the device with a separate 3.3-V supply.





By using version TPS272C45A and providing a 3.3-V supply to the VDD pin, for a 500-mA output module the worst case device total heating is cut from 250 mW to 89 mW, about a 30% decrease in per channel power dissipation. This lower power dissipation, in addition to the small size of the TPS272C45, enables modules that have many low current outputs to shrink the size of their casings without limiting output power distribution capability. To minimize power dissipation, the VDD supply must be powered by a small DC/DC providing the less than 5 mA per device. Multiple devices can use one DC/DC converter to limit system costs, as shown in  $\boxtimes$  9-6.







For higher current modules, the resistive losses dominate the total power dissipation and the impact of the secondary supply is less valuable. For example,  $\overline{x}$  9-3 shows that for a 2-A output, providing the secondary supply lowers the total device dissipation by only 12%. In this case, to lower total system costs, versions with an internal regulator that need only single supply input can be used. If using versions C or D and the secondary supply is not useful or available, the VDD pin can be grounded and all current is drawn from the primary supply with no loss of functionality, but higher power dissipation.

# **9.3.3 Protection Mechanisms**

The TPS272C45 protects the system against load fault events like short circuits, inductive load kickback, overload events, overvoltage and over-temperature events. This section describes the details for protecting against each of these fault cases.

There are a number of protection features which, if triggered, causes the switch to automatically disable:

- Current limit
- Thermal shutdown
- DC overvoltage on VS supply above the overvoltage protection threshold,  $V_{\text{OVPR}}$

When one of these protections are triggered for either channel, the device enters the FAULT state. In the FAULT state, the fault indication is available on the FLT pin for an MCU to monitor and react to.

The fault indication is reset and the switch turns back on when all of the below conditions are met:

• LATCH pin is low



- $t_{\text{RETRY}}$  has expired
- All faults are cleared (thermal shutdown, current limit, overvoltage)

# *9.3.3.1 Short-Circuit Protection*

TPS272C45 provides output short-circuit protection to ensure that the device prevents current flow in the event of a low impedance path to GND, removing the risk of damage or significant supply droop. The device is specified to protect against short-circuit events regardless of the state of the ILIM pins and or supply voltages up to 36V and across the entire opeprating temperature range -40 °C 125°C.

图 9-7 shows the behavior of the TPS272C45 when the device is enabled into an overload condition and then recovers to a normal load.



图 **9-7. Enable into Short-Circuit Behavior**

Due to the low impedance path, the output current rapidly increases until it hits the current limit threshold. Due to the response time of the current limiting circuit, the measured maximum current can temporarily exceed the  $I_{CL}$ value defined as  $I_{\text{Cl-ENPS}}$ , before it settles to the current limit regulation value ( $I_{\text{Cl}}$ ).

In this state high power is dissipated in the FET, so eventually the internal thermal protection temperature for the FET is reached and the device safely shuts down. Then if LATCH pin is low the part waits t<sub>RETRY</sub> amount of time and turns back on.

图 9-8 shows the behavior of the TPS272C45 when a short-circuit occurs when the device is in the on-state and already outputting current. When the internal pass FET is fully enabled, the current clamping settling time is slower so to ensure overshoot is limit, the device implements a fast trip turn-off at a high current threshold (approximately 40% higher than  $I_{CL}$ ). When this fast trip threshold is hit, the device shuts off after a delay for a short period of time before quickly re-enabling and clamping the current to the regulation current limit level  $(I_{CL})$ after a brief transient overshoot to the higher peak current level. The device then keeps the current clamped at the regulation current limit until the thermal shutdown temperature is hit and the device safely shuts off.



图 **9-8. On-State Short-Circuit Behavior**

Overload Behavior shows the behavior of the TPS272C45 when there is a small change in impedance that sends the load current above the  $I_{CL}$  threshold. The current rises to  $I_{CL-LIN}$  above the regulation level. Then the current limit regulation loop kicks in and the current drops to the  $I_{CL}$  value.



图 **9-9. Overload Behavior**

In all of these cases, the internal thermal shutdown is safe to hit repetitively. There is no device risk or lifetime reliability concerns from repeatedly hitting this thermal shutdown level.

# **9.3.3.1.1 VS During Short-to-Ground**

When  $V_{\text{OUT}}$  is shorted to ground, the module power supply ( $V_{\text{S}}$ ) can see a transient decrease. This decrease is caused by the sudden increase in current flowing through the cable inductance. For ideal system behavior, TI recommends that the module maintain V<sub>S</sub> > 3 V (above the maximum V<sub>UVLOF</sub>) during V<sub>OUT</sub> short-to-ground. This event is typically accomplished by placing bulk capacitance on the power supply node. If  $V_S$  goes below  $V_{UVLOF}$ , the device can sustain unexpected latch and timing behavior.

# *9.3.3.2 Inductive Load Demagnetization*

When switching off an inductive load, the inductor can impose a negative voltage on the output of the switch. The TPS272C45 includes voltage clamps between  $V_S$  and  $V_{OUT}$  to limit the voltage across the FETs and demagnetize load inductance if there is any. The negative voltage applied at the OUT pin drives the discharge of inductor current.  $\overline{8}$  9-10 shows the device discharging a 40-mH load.





图 **9-10. TPS272C45 Inductive Discharge (40 mH)**

The maximum acceptable load inductance is a function of the energy dissipated in the device and therefore the load current and the inductive load. The maximum energy and the load inductance the device can withstand for one pulse inductive dissipation at 125°C is shown in 图 9-11.The device can withstand 50% of this energy for one million inductive repetitive pulses with a >4-Hz repetitive pulse. If the application parameters exceed this device limit, use a protection device like a freewheeling diode to dissipate the energy stored in the inductor.







For more information on driving inductive loads, refer to TI's *How to Drive Inductive, Capacitive, and Lighting Loads With Smart High-Side Switches* application report.

#### *9.3.3.3 Thermal Shutdown*

The TPS272C45 includes a temperature sensor on the power FET and also within the controller portion of the device. The device registers a thermal shutdown fault:

- $\cdot$  T<sub>IFFT</sub> > T<sub>ABS</sub>
- $\bullet$   $T_{\text{J,FET}}$   $T_{\text{J,control}}$  >  $T_{\text{RFI}}$

After the fault is detected, the switch turns off. If  $T_{\text{J,FFT}}$  passes  $T_{\text{ABS}}$ , the fault is cleared when the switch temperature decreases by the hysteresis value,  $T_{HYS}$ . If instead the  $T_{REL}$  threshold is exceeded, the fault is cleared after  $T_{RFTRY}$  passes.

Each channel shuts down independently in case of a thermal event, as each has its own temperature sensor and fault reporting.

#### *9.3.3.4 Undervoltage Lockout on VS (UVLO)*

The device monitors the supply voltage at the VS pin to prevent unpredicted behaviors in the event that the supply voltage is too low. When the supply voltage falls down to  $V_{UVLOF}$ , the device enters the shut down state automatically. When the supply rises up to  $V_{UVLOR}$ , the device turns back on.

Fault is not indicated on the FLT pin during an UVLO event. During an initial ramp of  $V_{VS}$  from 0 V at a ramp rate slower than 1 V/ms,  $V_{ENx}$  pins must be held low until  $V_s$  is above the UVLO threshold. For best operation, ensure that  $V_S$  has risen above UVLO before setting the  $V_{ENx}$  pins to high.

#### *9.3.3.5 Undervoltage Lockout on Low Voltage Supply (VDD\_UVLO)*

The device monitors the input supply voltage  $V_{VDD}$  (in versions A/C/D with external supply input) to prevent unpredictable behavior in the event that the supply voltage is too low. When the supply voltage falls down to V<sub>VDD UVLOF</sub>, the device switches operation to the VS (24 V) power supply, but results in increased current draw from the VS supply input.

#### *9.3.3.6 Power-Up and Power-Down Behavior*

All versions of the device power up from the OFF state only when the VS supply input exceeds the V<sub>VSUVLOR</sub> threshold (independent of the VDD supply input level). When VS supply is above the threshold, the internal regulators are enabled, the device version is recognized. The device then enters the standby state. With versions A, C, and D and using using an external supply on VDD pin - the device will use the internal regulators until the VDD voltage exceeds  $V_{VDD-UVLOR}$ .

In case the VDD power supply is enabled first and the VDD voltage exceeds  $V_{VDD-UVLOR}$  before the VS supply is up and the VS voltage exceeds  $VS<sub>UVOR</sub>$ , the device remains in the off-state.

The behavior of all versions of the device in case of brown-out or power loss in VS supply is as described in *Undervoltage Lockout on VS (UVLO)*. For versions A, C, and D if the VDD power supply is lost (VDD supply voltage falls below  $V_{VDD\ UVLOR}$  threshold), the device switches over to the internal power supply, the switch outputs are disabled.

#### *9.3.3.7 Overvoltage Protection (OVPR)*

The device monitors the supply voltage  $V_{VS}$  to prevent higher voltages from appearing at the output than can be supported by the load, when the supply voltage is too high. When the supply voltage goes above  $V_{VS}$  <sub>OVPR</sub>, the FET is shut down automatically after a deglitch time to prevent short transients or noise from triggering the protection. When the supply falls below  $V_{VS-OVPF}$ , the FET is allowed to turn back on.

#### **9.3.4 Diagnostic Mechanisms**

As systems demand more intelligence, it is becoming increasingly important to have robust diagnostics measuring the conditions of output power. The TPS272C45 integrates many diagnostic features that enable modules to provide predictive maintenance and intelligence power monitoring to the system.



# *9.3.4.1 Current Sense*

The SNS output can be used to sense the load current through either channel. The SNS pin outputs a current that is proportional to the load current through either channel, depending on the state of the SEL pin. This current is sourced into an external resistor to create a voltage that is proportional to the load current. This voltage can be measured by an ADC or comparator and used to implement intelligent current monitoring for a system. To ensure accurate sensing measurement,  $R_{SNS}$  must be connected to the same ground potential as the μC ADC.

The SNS pin output is controlled by the SEL pin. If SEL pin is low, SNS outputs load current proportional to channel 1, whereas if SEL is high SNS outputs load current proportional to channel 2.

Equation 3 shows the transfer function for calculating the load current from the SNS pin current.

 $I_{SNSI} = I_{OUT} / K_{SNS}$  (2)

K<sub>SNS</sub> is defined in the *Specifications* section.

#### **9.3.4.1.1 RSNS Value**

The following factors must be considered when selecting the  $R_{SNS}$  value:

- Current sense ratio  $(K_{\text{SNS}})$
- Largest and smallest diagnosable load current required for application operation
- Full-scale voltage of the ADC
- Resolution of the ADC

For an example of selecting R<sub>SNS</sub> value, reference R<sub>ISNS</sub> Calculation in the applications section of this data sheet.

#### *9.3.4.1.1.1 Current Sense Output Filter*

To achieve the most accurate current sense value, TI recommends to filter the SNS output. There are two methods of filtering:

- Low-Pass RC filter between the SNS pin and the ADC input. This filter is illustrated in 图 10-1 with typical values for the resistor and capacitor. The designer must select a C<sub>SNS</sub> capacitor value based on system requirements. A larger value provides improved filtering but a smaller value allows for faster transient response.
- The ADC and microcontroller can also be used for filtering. TI recommends that the ADC collects several measurements of the SNS output. The median value of this data set must be considered as the most accurate result. By performing this median calculation, the microcontroller can filter out any noise or outlier data.

#### *9.3.4.2 Fault Indication*

The following faults are registered on the FLTx pin:

- FET thermal shutdown
- Active current regulation
- Thermal Shutdown caused by current limitation
- Open-load (FET OFF state only)

Open-load or short-to-supply are not indicated while the switch is enabled, although in on-state these conditions can still be detected through the sensed current (ISNS current). Hence, if there is a fault indication while the channel is enabled, then it must be either due to an overcurrent or overtemperature event. On the other hand, a fault indication while the output (FET) is disabled must be either due to an open load or output short-to-supply.

In versions A, B, C of the device, the open drain FLT pin output is a global fault output. FLT pin indicates a fault when one occurs in either channel. The FLT signal can be deactivated by toggling the EN input of the faulted channel and sequential toggling of ENx inputs can be used to determine the faulted channel. In versions A, B, C



of the device the SNS pin also indicates the fault status of the channel, provided the faulted channel is selected with the SEL pin.

In version D of the device, there are two (FLT1 and FLT2) pin outputs corresponding the presence of a fault in each channel. The independent FLTx signals can be used to easily determine the faulted channel. The FLTx signal is deactivated by toggling the EN input of the faulted channel. In version D of the device the SNS pin does not indicate the fault status of the channel, just the load current sense.

表 9-4 shows the states for both the SNS pin and the  $\overline{\text{FLT}}$  pins based on the fault states and ENx/SEL pin state (applies to versions A, B, C). By looking at these pins, it is possible to detect where the fault has occurred. The method to identify the channel that caused the FLT signal is as follows when an MCU is monitoring the SNS pin output. If the SNS is signaling a fault (with  $I_{SNSFH}$  current output) while SEL=LO, then the fault is in channel 1, whereas with SEL=HI, the fault is in channel 2. If SNS pin signals fault with SEL at either LO or HI, then both channels are faulted. As discussed earlier, the type of faults (whether it is overcurrent, overtemperature or openload) can be determined by the state of EN input in each channel. If the SNS pin output is not monitored, it is still possible to identify the channel that is faulted. To do this, the EN pin in each channel must be toggled (LO to HI or HI to LO as the case can be). If the fault indication on the  $\overline{FLT}$  pin is removed by toggling the EN input in a channel, then the fault is in that channel. If the fault indication does not go away with toggling EN input of both channels, then the fault is in both. The time duration for toggling the EN input must be kept below 10 us to ensure that there is no impact on the actual output of the channels.





 $(1)$   $\bar{\mathcal{R}}$  9-5 describes this behavior

While typically the SNS pin output corresponds to I<sub>LOAD</sub>, in a fault case the switch turns off and I<sub>LOAD</sub> goes to zero so the SNS behavior is modified in a fault case. In the event of a fault cases where SEL is monitoring the proper channel, the SNS pin outputs a voltage level corresponding to the fault type to enable improved diagnosis as shown in  $\bar{\mathcal{R}}$  9-5.

By looking at the combination of the ENx condition,  $\overline{FLT}$ , and SNS pins, it is possible to distinguish between fault states. Each channel has independent fault states, so the table below applies to CH1 when SEL = LO and CH2 when SEL = HI.

<b>Channel State</b>	<b>Fault Case</b>	<b>SNS</b>	FLT
Enabled	Regulating current past the initial inrush delay set by ILIMD resistor	<b>ISNSFH</b>	Low
	Short-to-supply/open-load		High
	$T_{\text{J}}$ overtemperature	<b>ISNSFH</b>	Low

表 **9-5. Distinguishing Different Fault Cases (Versions A, B, C)**



表 **9-5. Distinguishing Different Fault Cases (Versions A, B, C) (continued)**

In version D of the device the fault table is shown in  $\frac{1}{3}$  9-6. By looking at these pins, it is possible to detect which channel the fault has occurred. As discussed earlier, the type of faults (whether it is overcurrent, overtemperature or open\_load) can be determined by the state of EN input in each channel.

#### 表 **9-6. Device Fault Mux (Version D)**



#### **9.3.4.2.1 Fault Event Diagrams**

备注

All timing diagrams assume that the SEL pin is low to measure channel one behavior on the SNS pin. DIA\_EN and SEL pins have no effect on the FLT (versions A, B, C) or FLT1, FLT2 (version D) pin output.

The LATCH, SEL, DIA EN, and ENx pins are controlled by the user. The timing diagrams represent possible use-cases.

图 9-12 shows the device fault reporting behavior in the event of a fault in channel 2 (only) with LATCH and SEL pin set to LO. As shown, the fault signaling is deactivated when EN is toggled (in this case from HI to LO to HI). The faulted channel can be determined by toggling the EN pin with a short pulse (less than 10-us wide) that does not affect the output of the channel.





图 **9-12. FLT Pin Behavior (Versions A, B, C)**

图 9-13 shows the device fault reporting behavior in the event of an overcurrent fault when EN goes high. As shown, the fault signaling is active only after the initial inrush current limit phase is complete.



# 图 **9-13. FLT Pin Behavior With an Overcurrent Event On Channel Enable (Versions A, B,C)**

图 9-14 shows the device fault and retry behavior when there is a slow creep into an overcurrent event. As shown, the switch clamps the current until it hits thermal shutdown, and then the device remains latched off until the LATCH pin is low.





图 **9-14. Current Limit** – **Latched Behavior**



图 9-15 shows the behavior with LATCH tied to GND; hence, the switch retries after the fault is cleared and  $t_{\text{RETRY}}$  has expired.



图 **9-15. Current Limit** – **LATCH = 0**

When the switch retries after a shutdown event, the fault indication remains until V<sub>OUTx</sub> has risen to V<sub>VS</sub> - 1.8 V. After  $V_{\text{OUTX}}$  has risen, the FLT output is reset and current sensing is available. If there is a short-to-ground and  $V_{\text{OUT}}$  is not able to rise, the SNS fault indication remains indefinitely.  $\boxed{8}$  9-16 illustrates auto-retry behavior and provides a zoomed-in view of the fault indication during retry.

# 备注

 $\overline{\boxtimes}$  9-16 assumes that t<sub>RETRY</sub> has expired by the time that T<sub>J</sub> reaches the hysteresis threshold.

 $LATCH = LO$  and  $DIA$   $EN = HI$ 





# 图 **9-16. Fault Indication During Retry**



## *9.3.4.3 Short-to-Supply or Open-Load Detection*

The TPS272C45 is capable of detecting short-to-supply and open-load events regardless of whether the switch is turned on or off, however the two conditions use different methods to signify fault. This feature enables systems to recognize mis-wiring or wire-break events.

#### **9.3.4.3.1 Detection With Switch Enabled**

When the switch is enabled, the short-to-supply and open-load conditions are detected through the current sense feature. In both cases, the load current drops from the nominal value and instead be measured as close to zero. By measuring load current through the SNS pin, this state can be recognized.

#### **9.3.4.3.2 Detection With Switch Disabled**

While the switch is disabled and DIA\_EN high, an internal comparator watches the condition of  $V_{OUT}$ . The TPS272C45 includes a nominally 150-k Ω pull-up resistor from OUT pin to VS pin in series with a switch controlled by the DIA\_EN signal. So, if the load is disconnected (open load condition) or there is a short to supply the V<sub>OUT</sub> voltage is pulled towards V<sub>VS</sub>. In either of these events, the internal comparator measures V<sub>OUT</sub> as higher than the open load threshold ( $V_{\text{OL off}}$ ) and a fault is indicated on the FLT pin (Version A) or FLTx pins (Version D) and on the SNS pin (only for versions A, B, C). No external component is required in most cases, however if there is a pull-down resistor to GND on  $V_{\text{OUT}}$ , an additional external pull-up resistor can be necessary to bias  $V_{\text{OUT}}$  appropriately.

Open load fault signaling on the SNS and the internal pull-up on OUT is enabled only if DIA\_EN is set HI. To detect open-load threshold at higher pull-down load current, an external pull-up resistor (and potentially a switch) can be needed.

While the switch is disabled, the fault indication mechanisms continuously represent the present status. For example, if V<sub>OUT</sub> decreases from greater than V<sub>OL off</sub> to less than V<sub>OL off</sub>, the fault indication is reset. Additionally, the fault indication is reset upon the falling edge of DIA\_EN (for SNS pin) or the rising edge of EN.



图 **9-17. Open-Load Detection Circuit**





Copyright © 2019, Texas Instruments Incorporated

#### 图 **9-18. Open-Load Detection Timing**

# *9.3.4.4 Current Sense Resistor Sharing*

Multiple high-side devices can use the same R<sub>SNS</sub> as shown in  $\boxtimes$  9-19. This action reduces the total number of passive components in the system and the number of ADC terminals that are required of the microcontroller.





图 9-19. Sharing R<sub>SNS</sub> Among Multiple Devices

# **9.4 Device Functional Modes**

During typical operation, the TPS272C45 can operate in a number of states that are described below.

# **9.4.1 Off**

OFF state occurs when the device is not powered.

# **9.4.2 Diagnostic**

DIAGNOSTIC state occurs with DIA\_EN is high but ENx are both low. The switch can be used to perform diagnostics like off-state open-load detection in this state.

# **9.4.3 Active**

In ACTIVE state, the switch is enabled with ENx high. The diagnostic functions like current sense can be either on or off during ACTIVE state.

# **9.4.4 Fault**

The FAULT state is entered if a fault shutdown occurs (thermal shutdown or current limit). After all faults are cleared, the LATCH pin is low, and the retry timer has expired, the device transitions out of FAULT state. If the EN pin is high, the switch re-enables. If the EN pin is low, the switch remains off.



# **10 Application and Implementation**

备注

以下应用部分中的信息不属于 TI 器件规格的范围, TI 不担保其准确性和完整性。TI 的客 户应负责确定 器件是否适用于其应用。客户应验证并测试其设计,以确保系统功能。

# **10.1 Application Information**

 $\boxtimes$  10-1 shows the schematic of a typical application of the TPS272C45. The schematic includes all standard external components. This section of the data sheet discusses the considerations in implementing commonly required application functionality.

If reverse polarity can be applied to the VS supply voltage input, the ground network protection circuit must be added. The diode prevents the reverse current flow from the GND pin to supply. An additional resistor of 10 ohms or less is added to reduce the current flow if the VS to GND voltage rating is exceeded during any surge conditions. TI recommends the 1-K resistor in parallel to keep the GND potential close to the board GND under conditions where the ground network diode can be reverse biased.



Copyright © 2019, Texas Instruments Incorporated

图 **10-1. System Diagram**



#### 表 **10-1. Recommended External Components**

#### **10.1.1 IEC 61000-4-5 Surge**

The TPS272C45 is designed to survive against IEC 61000-4-5 surge using external TVS clamps. The device is rated to 48 V ensuring that external TVS diodes can clamp below the rated maximum voltage of the TPS272C45. Above 48 V, the device includes  $V_{DS}$  clamps to help shunt current and ensure that the device survives the transient pulses. Depending on the class of the output, TI recommends that the system has a SMBJ36A or SMCJ36A between VS and module GND.

#### **10.1.2 Inverse Current**

Inverse current occurs when  $0 \vee \vee \vee_{\vee S} \vee \vee_{\vee U} I$ . In this case, current can flow from VOUT to VS. Inverse current cannot be caused by a purely resistive load. However, a capacitive or inductive load can cause inverse current. For example, if there is a significant amount of load capacitance and the  $V_S$  node has a transient droop,  $V_{OUT}$ can be greater than  $V_{\rm S}$ .

The TPS272C45 does not detect inverse current. When the switch is enabled, inverse current passes through the switch. When the switch is disabled, inverse current can pass through the MOSFET body diode. The device continues operating in the normal manner during an inverse current event.

#### **10.1.3 Loss of GND**

The ground connection can be lost either on the device level or on the module level. If the ground connection is lost, both the channel outputs are disabled irrespective of the EN input level. If the switch was already disabled when the ground connection was lost, the outputs remain disabled even when the channels are enabled. The steady state current from the output to the load that remains connected to the system ground is below the level specified in the *Specifications* section of this document. When the ground is reconnected, normal operation resumes.

#### **10.1.4 Paralleling Channels**

If an application requires lower power dissipation than is possible with a 45-mΩ switch, the TPS272C45 can have both channel outputs and ENx pins tied together to function as a single 22.5-m Ω high side switch. In this case, there is some decrease in  $I_{SNS}$  and  $I_{LIM}$  accuracy, however the device functions properly.

#### **10.1.5 Thermal Information**

When outputting current, the TPS272C45 heats up due to the power dissipation. The transient thermal impedance curve can be used to determine the device temperature during a pulse current of a given duration (time). This Z  $_{\theta$  JA value here corresponds to a JEDEC standard 2s2p thermal test PCB with no thermal vias.

#### Copyright © 2022 Texas Instruments Incorporated *Submit Document Feedback* 41





图 **10-2. TPS272C45 Transient Thermal Impedance**



# **10.2 Typical Application**

This application example demonstrates how the TPS272C45 device can be used as output switches in a digital output module. In this example, consider an 8-channel module with a maximum output current capability of 2 A per channel.



图 **10-3. Block Diagram for PLC Digital Output Module**

# **10.2.1 Design Requirements**

For this design example, use the input parameters shown in  $\bar{\mathcal{R}}$  10-2.



# 表 **10-2. Design Parameters**

#### **10.2.2 Detailed Design Procedure**

#### *10.2.2.1 RILIM Calculation*

In this application, the TPS272C45 must allow for the maximum DC current with margin but minimize the energy in the switch and the load on the input supply during a fault condition by minimizing the current limit.



The nominal current limit must be set such that the worst case (lowest) current limit is higher than the maximum load current (2 A). Because the lower limit is 23% below the typical value, for this application, the best  $I_{LIM}$  set point is approximately 2.6 A for both channels. The below equation allows you to calculate the R<sub>ILIM</sub> value that is placed from the I<sub>LIMx</sub> pins to GND pin of the device. R<sub>ILIM</sub> is calculated in k Ω.

$$
R_{\text{ILIM}} = K_{\text{CL}} / I_{\text{CL}} \tag{3}
$$

The K<sub>CL</sub> value in the *Specifications* section is 20.5 A × k Ω . So the calculated value of R<sub>ILIM</sub> closest 2% resistor is 7.87 kΩ.

# *10.2.2.2 Diagnostics*

If the load is disconnected due a break in the connecting wire, an alert is desired. Open-load detection can be performed in the switch-enabled state with the current sense feature of the TPS272C45 device. Similarly in the off-state, a check for wire break can be performed. Under open load condition, with the DIA\_EN set high, the current in the SNS pin is the fault current and the can be detected from the sense voltage measurement.

#### **10.2.2.2.1 Selecting the RISNS Value**

表 10-3 shows the requirements for the load current sense in this application. The K<sub>SNS</sub> value is specified for the device and can be found in the *Specifications* section.





The load current measurement up to 2.4 A ensures that even in the event of a overcurrent but below the set current limit, the MCU can register and react by turning off the FET while the low level of 50 mA allows for accurate measurement of low load currents and enable the distinction open load faults from nominal load currents.

The R<sub>SNS</sub> resistor value can be selected such that the largest diagnosable load current puts the SNS pin voltage  $(V_{\text{SNS}})$  less than the ADC full-scale. With this design, any ADC value that shows full scale (FS) can be considered a fault. Additionally, the  $R_{SNS}$  resistor value must ensure that the smallest diagnosable load current does not cause V<sub>SNS</sub> to fall below at a least a few LSB of the ADC. With the given example values, a 2.4-kΩ sense resistor satisfies both requirements shown in  $\frac{1}{\sqrt{6}}$  10-4.







#### **10.2.3 Application Curves**

Upon enabling our device into a capacitive load, TPS272C45 defaults its current limit to 2x ICL for a period of time programmed set by ILIMD. In the figure below, you can see TPS272C45 charging a 1-mF capacitor using the inrush current handling feature. During the first 4 mS after enabling the device, IOUT1 is 2 times the icl programmed (4 A). After, the 4-mS period, the current folds back to the programmed icl (2 A).



![](_page_44_Figure_5.jpeg)

If the device has a no-load case due to an open load or wire-break, the device registers the fault even in an offstate if the DIA\_EN pin is high.  $[8]$  10-5 shows the device behavior when an open load event is registered with EN low and DIAG\_EN is raised. Systems can PWM DIA\_EN to lower system power losses while still watching for open load events and the same timing applies.

![](_page_45_Picture_1.jpeg)

![](_page_45_Figure_2.jpeg)

# 图 **10-5. Open-Load (tOL) Detection Time**

If the output of the TPS272C45 is short-circuited, the device protects the system from failure. Depending on  $R_{\text{lLIM}}$ , the current limit set-point varies. The waveforms below show examples of the current limit behavior when the device is enabled into a short circuit.

In the Figure 10-6, the output is permanently shorted. Upon enabling the device, the current reaches the 2 times current limit is enabled for 6 mS set by ILIMD resistor. After the inrush current period, the current is reduced to the programmed current limit set by  $R_{I L I M.}$  In this case, because the power dissipation is low enough, the device is able to constantly act as a current source.

![](_page_45_Figure_6.jpeg)

图 **10-6. Enabling into Short (RILIM = 10 k , VS = 6 V, Delay = 6 mS)**

In Figure 10-7, the output is also permanently shorted. Upon enabling the device, the current reaches the 2 times current limit, however because the power dissipation is greater due to the higher input voltage at Vs the device reaches its thermal shutdown threshold and disables itself before reaching the programmed delay time.

![](_page_46_Figure_3.jpeg)

图 **10-7. Enabling into Short (RILIM = 10 k , VS = 24 V, Delay = 6 mS)**

The Figure 10-8 shows that after the device has been enabled into a short and due to the high power dissipation, the device reaches its thermal shutdown threshold. The device then shuts down the FET for a period of tRETRY and re-enables the FET into the short. The capture shows the continuous retry cycle and protection because the short is permanently applied.

![](_page_46_Figure_6.jpeg)

图 **10-8. Permanent Short Behavior (RILIM = 10 k , VS = 24 V, Delay = 6 mS)**

![](_page_47_Picture_1.jpeg)

In the event a short is applied to the output while a load is being driven, the device activates its fast trip comparator and shutdown the output to limit the inrush current. The device then immediately re-enables into the short and limit the current to the programmed current limit value. The figure below describes the described behavior.

![](_page_47_Figure_3.jpeg)

图 10-9. On-State Short circuit (R<sub>ILIM</sub> = 10 k, V<sub>S</sub> = 24 V)

# **11 Power Supply Recommendations**

The TPS272C45 device is designed to operate in a 24-V industrial system. The allowed supply voltage range (VS pin) is 6 V to 36 V as measured at the VSpin with respect to the GND pin of the device. In this range the device meets full parametric specifications as listed in the *Electrical Characteristics* table. The maximum continuous operating voltage is 36 V. The device is also designed to withstand voltage transients beyond this range. The device version A requires an external power supply input in the range 3.0 V to 5.5 V. The C and D versions of the device have an secondary internal regulator (nominally 3.3 V) but an external supply can be optionally provided at the VDD pin to lower the power dissipation in the IC. Version B always use an internal 3.3V regulator, so a single 24V supply (VS pin) is sufficient.

![](_page_47_Picture_144.jpeg)

![](_page_47_Picture_145.jpeg)

![](_page_48_Picture_0.jpeg)

# **12 Layout**

# **12.1 Layout Guidelines**

To achieve optimal thermal performance, connect the exposed pad to a large copper pour. On the top PCB layer, the pour can extend beyond the package dimensions as shown in the example below. In addition to this, TI recommends to also have a GND plane either on one of the internal PCB layers or on the bottom layer.

Vias must connect this plane to the top GND pour.

Ensure that all external components are placed close to the pins. Device current limiting performance can be harmed if the  $R_{\text{lLM}}$  is far from the pins and extra parasitics are introduced.

#### **12.2 Layout Example**

![](_page_48_Figure_8.jpeg)

# 图 **12-1. Layout Example**

![](_page_49_Picture_1.jpeg)

# **13 Device and Documentation Support**

# **13.1 Documentation Support**

# **13.1.1 Related Documentation**

- Texas Instruments, *Adjustable Current Limit of Smart Power Switches* application report
- Texas Instruments, *How to Drive Inductive, Capacitive, and Lighting Loads With Smart High-Side Switches*  application report

# **13.2** 接收文档更新通知

要接收文档更新通知,请导航至 ti.com 上的器件产品文件夹。点击*订阅更新* 进行注册,即可每周接收产品信息更 改摘要。有关更改的详细信息,请查看任何已修订文档中包含的修订历史记录。

# **13.3** 支持资源

TI E2E™ 支持论坛是工程师的重要参考资料,可直接从专家获得快速、经过验证的解答和设计帮助。搜索现有解 答或提出自己的问题可获得所需的快速设计帮助。

链接的内容由各个贡献者"按原样"提供。这些内容并不构成 TI 技术规范,并且不一定反映 TI 的观点;请参阅 TI 的《使用条款》。

# **13.4 Trademarks**

TI E2E™ is a trademark of Texas Instruments.

所有商标均为其各自所有者的财产。

#### **13.5 Electrostatic Discharge Caution**

![](_page_49_Picture_16.jpeg)

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

# **13.6** 术语表

TI 术语表 本术语表列出并解释了术语、首字母缩略词和定义。

![](_page_50_Picture_0.jpeg)

# **14 Mechanical, Packaging, and Orderable Information**

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

![](_page_51_Picture_0.jpeg)

# **PACKAGING INFORMATION**

![](_page_51_Picture_288.jpeg)

**(1)** The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

<sup>(2)</sup> RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the  $\leq$  1000ppm threshold requirement.

**(3)** MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

**(4)** There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

**(5)** Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

**(6)** Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

**Important Information and Disclaimer:**The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and

![](_page_52_Picture_0.jpeg)

continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

![](_page_53_Picture_1.jpeg)

**TEXAS** 

# **TAPE AND REEL INFORMATION**

**STRUMENTS** 

![](_page_53_Figure_4.jpeg)

\*All dimensions are nominal

![](_page_53_Figure_5.jpeg)

#### **QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**

![](_page_53_Figure_7.jpeg)

![](_page_53_Picture_313.jpeg)

![](_page_54_Picture_0.jpeg)

www.ti.com 3-Jun-2022

# **PACKAGE MATERIALS INFORMATION**

![](_page_54_Figure_4.jpeg)

\*All dimensions are nominal

![](_page_54_Picture_122.jpeg)

![](_page_55_Picture_1.jpeg)

# **PACKAGE OUTLINE**

# **RHF0024A VQFN - 1 mm max height**

PLASTIC QUAD FLATPACK - NO LEAD

![](_page_55_Figure_5.jpeg)

#### NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

![](_page_55_Picture_10.jpeg)

# **EXAMPLE BOARD LAYOUT**

# **RHF0024A VQFN - 1 mm max height**

PLASTIC QUAD FLATPACK - NO LEAD

![](_page_56_Figure_4.jpeg)

4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).

5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.

![](_page_56_Picture_7.jpeg)

# **EXAMPLE STENCIL DESIGN**

# **RHF0024A VQFN - 1 mm max height**

PLASTIC QUAD FLATPACK - NO LEAD

![](_page_57_Figure_4.jpeg)

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

![](_page_57_Picture_7.jpeg)

# 重要声明和免责声明

TI"按原样"提供技术和可靠性数据(包括数据表)、设计资源(包括参考设计)、应用或其他设计建议、网络工具、安全信息和其他资源, 不保证没有瑕疵且不做出任何明示或暗示的担保,包括但不限于对适销性、某特定用途方面的适用性或不侵犯任何第三方知识产权的暗示担 保。

这些资源可供使用 TI 产品进行设计的熟练开发人员使用。您将自行承担以下全部责任:(1) 针对您的应用选择合适的 TI 产品,(2) 设计、验 证并测试您的应用,(3) 确保您的应用满足相应标准以及任何其他功能安全、信息安全、监管或其他要求。

这些资源如有变更,恕不另行通知。TI 授权您仅可将这些资源用于研发本资源所述的 TI 产品的应用。严禁对这些资源进行其他复制或展示。 您无权使用任何其他 TI 知识产权或任何第三方知识产权。您应全额赔偿因在这些资源的使用中对 TI 及其代表造成的任何索赔、损害、成 本、损失和债务,TI 对此概不负责。

TI 提供的产品受 TI 的销售条款或 ti.com 上其他适用条款/TI 产品随附的其他适用条款的约束。TI 提供这些资源并不会扩展或以其他方式更改 TI 针对 TI 产品发布的适用的担保或担保免责声明。

TI 反对并拒绝您可能提出的任何其他或不同的条款。

邮寄地址:Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2022,德州仪器 (TI) 公司

# **X-ON Electronics**

Largest Supplier of Electrical and Electronic Components

*Click to view similar products for* [Power Switch ICs - Power Distribution](https://www.xonelec.com/category/semiconductors/integrated-circuits-ics/switch-ics/power-switch-ics-power-distribution) *category:*

*Click to view products by* [Texas Instruments](https://www.xonelec.com/manufacturer/texasinstruments) *manufacturer:* 

Other Similar products are found below :

[TLE6232GP](https://www.xonelec.com/mpn/infineon/tle6232gp) [NCP45520IMNTWG-L](https://www.xonelec.com/mpn/onsemiconductor/ncp45520imntwgl) [VND5E004ATR-E](https://www.xonelec.com/mpn/stmicroelectronics/vnd5e004atre) [FPF1018](https://www.xonelec.com/mpn/onsemiconductor/fpf1018) [DS1222](https://www.xonelec.com/mpn/analogdevices/ds1222) [NCV380HMUAJAATBG](https://www.xonelec.com/mpn/onsemiconductor/ncv380hmuajaatbg) [SZNCP3712ASNT3G](https://www.xonelec.com/mpn/onsemiconductor/szncp3712asnt3g) [NCP45520IMNTWG-H](https://www.xonelec.com/mpn/onsemiconductor/ncp45520imntwgh) [VND5004ATR-E](https://www.xonelec.com/mpn/stmicroelectronics/vnd5004atre) [AP22811BW5-7](https://www.xonelec.com/mpn/diodesincorporated/ap22811bw57) [SLG5NT1437VTR](https://www.xonelec.com/mpn/silego/slg5nt1437vtr) [SZNCP3712ASNT1G](https://www.xonelec.com/mpn/onsemiconductor/szncp3712asnt1g) [DML1008LDS-7](https://www.xonelec.com/mpn/diodesincorporated/dml1008lds7) [TS13011-QFNR](https://www.xonelec.com/mpn/semtech/ts13011qfnr) [VND7012AYTR](https://www.xonelec.com/mpn/stmicroelectronics/vnd7012aytr) [NCV459MNWTBG](https://www.xonelec.com/mpn/onsemiconductor/ncv459mnwtbg) [NCP4545IMNTWG-L](https://www.xonelec.com/mpn/onsemiconductor/ncp4545imntwgl) [NCV8412ASTT1G](https://www.xonelec.com/mpn/onsemiconductor/ncv8412astt1g) [NCV8412ASTT3G](https://www.xonelec.com/mpn/onsemiconductor/ncv8412astt3g) [FPF2260ATMX](https://www.xonelec.com/mpn/onsemiconductor/fpf2260atmx) [SLG5NT1765V](https://www.xonelec.com/mpn/dialogsemiconductor/slg5nt1765v) [SLG5NT1757V](https://www.xonelec.com/mpn/dialogsemiconductor/slg5nt1757v) [NCP45780IMN24RTWG](https://www.xonelec.com/mpn/onsemiconductor/ncp45780imn24rtwg) [AP2151DMPG-13](https://www.xonelec.com/mpn/diodesincorporated/ap2151dmpg13) [AP2151AMP-13](https://www.xonelec.com/mpn/diodesincorporated/ap2151amp13) [NCP45540IMNTWG-L](https://www.xonelec.com/mpn/onsemiconductor/ncp45540imntwgl) [TPS2022P](https://www.xonelec.com/mpn/texasinstruments/tps2022p) [FPF2495BUCX](https://www.xonelec.com/mpn/onsemiconductor/fpf2495bucx) [NCP45650IMNTWG](https://www.xonelec.com/mpn/onsemiconductor/ncp45650imntwg) [NCV8412ADDR2G](https://www.xonelec.com/mpn/onsemiconductor/ncv8412addr2g) [DK5V100R20S](https://www.xonelec.com/mpn/dongke/dk5v100r20s) [BTS7020-2EPA](https://www.xonelec.com/mpn/infineon/bts70202epa) [BTT6100-2ERA](https://www.xonelec.com/mpn/infineon/btt61002era) [BTS71220-4ESA](https://www.xonelec.com/mpn/infineon/bts712204esa) [DK5V100R15M](https://www.xonelec.com/mpn/dongke/dk5v100r15m) [WS3220C9-9/TR](https://www.xonelec.com/mpn/willsemiconductor/ws3220c99tr) [BTT6030-2ERA](https://www.xonelec.com/mpn/infineon/btt60302era) [TLE75602-ESH](https://www.xonelec.com/mpn/infineon/tle75602esh) [BTS5200-4EKA](https://www.xonelec.com/mpn/infineon/bts52004eka) [DK5V150R25M](https://www.xonelec.com/mpn/dongke/dk5v150r25m) [DK5V45R25](https://www.xonelec.com/mpn/dongke/dk5v45r25) [DK5V100R25S](https://www.xonelec.com/mpn/dongke/dk5v100r25s) [AW35206FOR](https://www.xonelec.com/mpn/awinic/aw35206for) [BTS7120-2EPA](https://www.xonelec.com/mpn/infineon/bts71202epa) [TLE75008-ESD](https://www.xonelec.com/mpn/infineon/tle75008esd) [BTS7040-1EPA](https://www.xonelec.com/mpn/infineon/bts70401epa) [BTT6030-1ERA](https://www.xonelec.com/mpn/infineon/btt60301era) [DK5V60R10S](https://www.xonelec.com/mpn/dongke/dk5v60r10s) [DK5V45R25S](https://www.xonelec.com/mpn/dongke/dk5v45r25s) [DK5V60R10](https://www.xonelec.com/mpn/dongke/dk5v60r10)