# **Not Recommended for New Designs**

# **ZVS Regulators**

PI358x-00



# 30 – 60V<sub>IN</sub> ZVS Buck Regulator

## **Product Description**

The PI358x-00 is a family of high input voltage, wide-input-range DC-DC ZVS Buck regulators integrating controller and power switches within a high-density GQFN (UTAC's Grid-array QFN) package.

The integration of a high-performance Zero-Voltage Switching (ZVS) topology, within the PI358x-00 series, increases point-of-load performance providing best-in-class power efficiency.

Device	Out	I May	
Device	Set	Range	I <sub>OUT</sub> Max
PI3583-00-QFYZ	3.3V	2.2 – 4.0V	10A
PI3585-00-QFYZ	5.0V	3.8 – 6.5V	10A
PI3586-00-QFYZ	12.0V	6.5 – 14V	9A



#### **Features & Benefits**

- High-Efficiency HV ZVS Buck Topology
- Wide input voltage range of 30 60V
- Power up into pre-biased load < 6V
- Parallel capable with single-wire current sharing
- Input Over/Undervoltage Lockout (OVLO/UVLO)
- Output Overvoltage Protection (OVP)
- Overtemperature Protection (OTP)
- Fast and slow current limits
- · Differential amplifier for output remote sensing
- User adjustable soft start & tracking
- –20 to 120°C operating range (T<sub>INT</sub>)

## **Applications**

- HV to PoL Buck Regulator Applications
- Computing, Communications, Industrial, Automotive Equipment

## **Package Information**

• 37-Pin GQFN



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## **Order Information**

Product	Nominal Output	Rated I <sub>OUT</sub>	Package	Transport Media
PI3583-00-QFYZ	3.3V	10A	7 x 8mm GQFN	TRAY
PI3585-00-QFYZ	5.0V	10A	7 x 8mm GQFN	TRAY
PI3586-00-QFYZ	12.0V	9A	7 x 8mm GQFN	TRAY

# **Thermal, Storage and Handling Information**

Name	Rating
Storage Temperature	−65 to 150°C
Internal Operating Temperature	−20 to 120°C
Soldering Temperature for 30 seconds	260°C
MSL Rating	MSL3
ESD Rating, JESD22-A114F, JS-002-2014	500V HBM; 200V CDM, respectively

# **Absolute Maximum Ratings** [a]

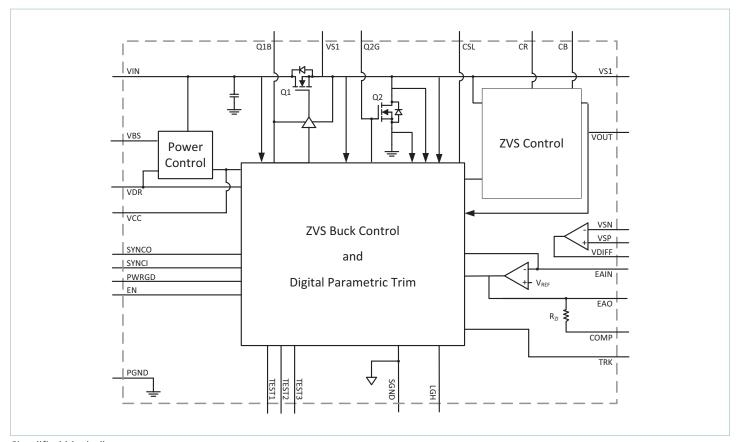
Name	Rating
VIN	-0.7 to 75V
VS1	-6 <sup>[b]</sup> to 75V
VOUT	-0.5 to 25V
CR	-0.7 to 25V
СВ	–0.3 to 5.5V with respect to CR
Q1B	-0.3 to 5.5V with respect to VS1
VBS	-0.7 to 75V
Q2G	-0.5 to 5.5V
SGND	±100mA
TRK	-0.3 to 5.5V, ±30mA
VDR, VCC, SYNCI, SYNCO, PWRGD, EN, CC, CSL, COMP, EAO, EAIN, VDIFF, VSN, VSP, TESTx	-0.3 to 5.5V, ±5mA

<sup>[</sup>a] Stresses beyond these limits may cause permanent damage to the device. Operation at these conditions or conditions beyond those listed in the Electrical Specifications table is not guaranteed. All voltages are referenced to PGND unless otherwise noted.



<sup>[</sup>b] Peak during switching transient.

# **Functional Block Diagram**



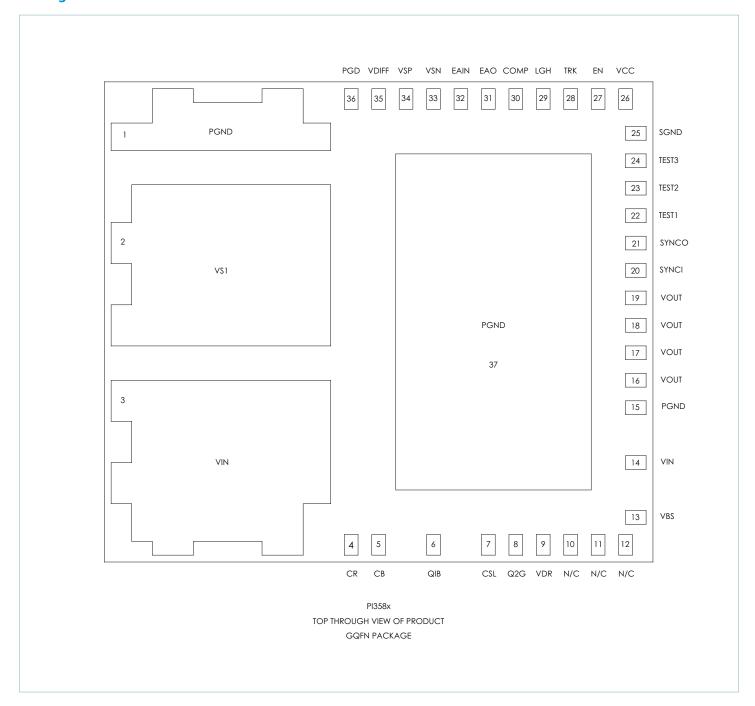
Simplified block diagram

# **Pin Description**

Name	Location	I/O	Description
PGND	1, 15, 37	Power	Power Ground: VIN and VOUT power returns
VS1	2	Power	<b>Switching Node:</b> and ZVS sense for power switches. Requires a schottky diode clamp with a low inductance connection in parallel with an RC snubber for 1nF and $0.3\Omega$ . Refer to Table 1 for the recommended components.
VIN	3	Power	Input Voltage: for the power stage.
VIIV	14	Power	Input Voltage: and sense for UVLO, OVLO and feed forward ramp.
CR	4	Power	ZVS control function node. Requires a 40V schottky diode clamp to PGND. Refer to Table 1 for the recommended component.
СВ	5	Power	ZVS control function node. Decouple with a 0.047µF capacitor between CB and CR. Refer to Table 1 for the recommended component.
Q1B	6	Power	Q1 driver boost pin. Decouple with a $0.22\mu F$ capacitor in series with a $1.3\Omega$ resistor between Q1B and VS1. Refer to Table 1 for the recommended components.
CSL	7	Power	ZVS control function node. Connect to PGND.
Q2G	8	Power	Q2 gate drive. Leave open.
VDR	9	I/O	<b>Gate Driver VCC:</b> 5.1V gate driver bias supply. May be used as a bias supply for low power external loads. See Application Description for important considerations.
N/C	10-12	I/O	No Internal connection.
VBS	13	Power	Switching node for gate driver bias supply.
VOUT	16-19	Power	Output Voltage: Internal Clamp connection and sense for power switches and feed-forward ramp.
SYNCI	20	I	<b>Synchronization Input:</b> Synchronize to the falling edge of external clock frequency. SYNCI is a high impedance digital input node and should always be connected to SGND when not in use. The PI358x-00 family is not optimized for external synchronization functionality.
SYNCO	21	0	<b>Synchronization Output:</b> Outputs a high signal at the start of each clock cycle for the longer of ½ of the minimum period or the on time of the high-side power MOSFET.
TEST1	22	I/O	Factory Test: Use only with factory guidance. Connect to SGND for proper operation.
TEST2	23	I/O	Factory Test: Use only with factory guidance. Connect to SGND for proper operation.
TEST3	24	I/O	Factory Test: Use only with factory guidance. Leave open.
SGND	25	VO	<b>Signal Ground:</b> Internal logic ground for EAO, EAIN, TRK, SYNCI, SYNCO communication returns. SGND and PGND are not connected inside the package. SGND should be connected to the large PGND island (controller paddle, pin 37) directly under the PI358x package. Sensitive analog nodes should be connected to the SGND side of the connection.
VCC	26	1/0	Control Circuitry VCC: Analog & digital bias. Decouple with 2.2µF to SGND.
EN	27	I/O	<b>Enable Input:</b> Regulator enable control. Asserted high or left floating – regulator enabled; Asserted low – regulator output disabled.
TRK	28	I	<b>Soft Start and Track Input:</b> An external capacitor with minimum capacitance of 47nF is required to be connected between TRK pin and SGND to control the rate of rise during soft start.
LGH	29	I/O	For factory use only. Connect to SGND in application.
СОМР	30	0	<b>Compensation Capacitor:</b> Connect capacitor for control loop dominant pole. See Error Amplifier section for details. A default C <sub>COMP</sub> of 4.7nF is used in the example.
EAO	31	0	Error Amplifier Output: External connection for additional compensation and current sharing.
EAIN	32	I	Error Amplifier Inverting Input: Connection for the feedback divider tap.
VSN	33	I	Independent Amplifier Inverting Input: If unused connect in unity gain.
VSP	34	I	Independent Amplifier Non-Inverting Input: If unused connect to SGND.
VDIFF	35	0	Independent Amplifier Output: Active only when module is enabled.
PWRGD	36	0	<b>Power Good:</b> High impedance when regulator is operating and VOUT is in regulation. Otherwise pulls to SGND.



# **Package Pinout**





## PI358x-00 Common Electrical Characteristics

Parameter	Symbol	Conditions	Min	Тур	Max	Unit
		Differential Amp				
Open Loop Gain		[d]	96	120	140	dB
Small Signal Gain-Bandwidth		[d]	5	7	12	MHz
Input Offset Error				0.5	1	mV
Common-Mode Input Range			-0.1		2.5	V
Differential-Mode Input Range					2	V
Input Bias Current			-1		1	μΑ
Sink/Source Current			-1		1	mA
Maximum V <sub>OUT</sub>		$I_{VDIFF} = -1mA$	4.85			V
Minimum V <sub>OUT</sub>		$I_{VDIFF} = -1mA$			20	mV
Capacitive Load Range for Stability		(j)	0		50	pF
Slew Rate				11		V/µs
		PWRGD				
V <sub>OUT</sub> Rising Threshold	V <sub>PG_HI%</sub>		78	84	90	% V <sub>OUT_DC</sub>
V <sub>OUT</sub> Falling Threshold	V <sub>PG_LO%</sub>		75	81	87	% V <sub>OUT_DC</sub>
PWRGD Output Low	V <sub>PG_SAT</sub>	Sink = 4mA			0.4	V

<sup>[</sup>c] All parameters reflect regulator and inductor system performance. Measurements were made using a standard PI358x evaluation board with 3 x 3in dimensions and 4 layer, 2oz copper. Refer to inductor pairing table within Application Description section for specific inductor manufacturer and value.



<sup>&</sup>lt;sup>[d]</sup> Regulator is assured to meet performance specifications by design, test correlation, characterization, and/or statistical process control. Output voltage is determined by an external feedback divider ratio.

<sup>[</sup>e] Output current capability may be limited and other performance may vary from noted electrical characteristics when V<sub>OUT</sub> is not set to nominal.

<sup>[</sup>f] Refer to Output Ripple plots.

<sup>[</sup>g] Refer to Load Current vs. Ambient Temperature curves.

<sup>[</sup>h] Refer to Switching Frequency vs. Load current curves.

<sup>[</sup>i] Contact factory applications for array derating and layout best practices to minimize sharing errors.

<sup>[</sup>j] Informational only.

## PI358x-00 Common Electrical Characteristics (Cont.)

Parameter	Symbol	Conditions	Min	Тур	Max	Unit
		VDR				
Voltage Set Point	$V_{VDR}$	$V_{IN\_DC} > 10V$	4.9	5.05	5.2	V
External Loading	$I_{VDR}$	See Application Description for details	0		2	mA
External Inductor Between VDR and VBS	L <sub>VBS</sub>	External required components for VDR, recommended to be an Inductor. Refer to Table 1 for the recommended component.		10		μΗ
External Capacitor Between VDR and PGND	$C_VDR$	External required components for VDR, recommended to be a capacitor. Refer to Table 1 for the recommended component.		2.2		μF
		Enable				
High Threshold	V <sub>EN_HI</sub>		0.9	1.0	1.1	V
Low Threshold	V <sub>EN_LO</sub>		0.7	0.8	0.9	V
Threshold Hysteresis	V <sub>EN_HYS</sub>		100	200	300	mV
Pull-Up Voltage Level for Source Current	V <sub>EN_PU</sub>			2		V
Pull-Up Current	I <sub>EN_PU_POS</sub>			50		μA
		Reliability				
MATRE		MIL-HDBK-217, 25°C, Ground Benign: GB		22.7		MHrs
MTBF		Telcordia SR-332, 25°C, Ground Benign: GB		191		MHrs

<sup>[</sup>c] All parameters reflect regulator and inductor system performance. Measurements were made using a standard Pl358x evaluation board with 3 x 3in dimensions and 4 layer, 2oz copper. Refer to inductor pairing table within Application Description section for specific inductor manufacturer and value.



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<sup>[</sup>f] Refer to Output Ripple plots.

<sup>[</sup>g] Refer to Load Current vs. Ambient Temperature curves.

<sup>&</sup>lt;sup>[h]</sup> Refer to Switching Frequency vs. Load current curves.

<sup>&</sup>lt;sup>[i]</sup> Contact factory applications for array derating and layout best practices to minimize sharing errors.

<sup>[</sup>j] Informational only.

Parameter	Symbol	Conditions	Min	Тур	Max	Unit
		Input Specifications		I	I	I
Input Voltage	V <sub>IN_DC</sub>		30	48	60	V
Input Current	I <sub>IN_DC</sub>	$V_{IN} = 48V$ , $T_{CASE} = 25$ °C, full load		0.77		А
Input Current at Output Short (Fault Condition Duty Cycle)	I <sub>IN_Short</sub>	Short at terminals		3		mA
Input Quiescent Current	I <sub>Q_VIN</sub>	Disabled		0.65		mA
Input Quiescent Current	I <sub>Q_VIN</sub>	Enabled, no load, T <sub>CASE</sub> = 25°C		1.8		mA
Input Voltage Slew Rate	V <sub>IN_SR</sub>				1	V/µs
		Output Specifications				
EAIN Voltage Total Regulation	V <sub>EAIN</sub>	[d]	0.975	0.990	1.005	V
Output Voltage Trim Range	V <sub>OUT_DC</sub>	[d] [e]	2.2	3.3	4.0	V
Line Regulation	ΔV <sub>OUT</sub> / ΔV <sub>IN</sub>	@ 25°C, 30V < V <sub>IN</sub> < 60V		0.10		%
Load Regulation	ΔV <sub>OUT</sub> / ΔI <sub>OUT</sub>	@ 25°C, 10% to 100% load		0.10		%
Output Voltage Ripple	V <sub>OUT_AC</sub>	Full load, $C_{OUT} = 6 \times 100 \mu F$ , 20MHz BW <sup>[f]</sup>		53		mV <sub>P-P</sub>
Output Current	I <sub>OUT_DC</sub>	[9]	0		10	А
Current Limit	I <sub>OUT_CL</sub>	Typical current limit based on nominal 420nH inductor.		11.5		А
Maximum Array Size	N <sub>PARALLEL</sub>	[d]			3	Modules
Output Current, Array of 2	I <sub>OUT_DC_ARRAY2</sub>	Total array capability, [d] see applications section for details	0		[i]	А
Output Current, Array of 3	I <sub>OUT_DC_ARRAY3</sub>	Total array capability, <sup>[d]</sup> see applications section for details	0		[i]	А
		Protection				
Input UVLO Start Threshold	V <sub>UVLO_START</sub>			27.0	29.1	V
Input UVLO Stop Hysteresis	V <sub>UVLO_HYS</sub>		1.66	2.08	2.50	V
Input UVLO Response Time				1.25		μs
Input OVLO Stop Threshold	V <sub>OVLO_STOP</sub>	[d]		64.3		V
Input OVLO Start Hysteresis	V <sub>OVLO_HYS</sub>	Hysteresis active when OVLO present for at least $t_{\text{FR\_DLY}}^{}$		1.17		V
Input OVLO Start Threshold	V <sub>OVLO_START</sub>	[d]	60.5			V
Input OVLO Response Time	t <sub>f</sub>			1.25		μs
Output Overvoltage Protection, Relative	V <sub>OVP_REL</sub>	Above set V <sub>OUT</sub>		20		%
Output Overvoltage Protection, Absolute	V <sub>OVP_ABS</sub>		4.8	5.3		V

<sup>[</sup>c] All parameters reflect regulator and inductor system performance. Measurements were made using a standard Pl358x evaluation board with 3 x 3in dimensions and 4 layer, 2oz copper. Refer to inductor pairing table within Application Description section for specific inductor manufacturer and value.



<sup>[</sup>d] Regulator is assured to meet performance specifications by design, test correlation, characterization, and/or statistical process control. Output voltage is determined by an external feedback divider ratio.

<sup>[</sup>e] Output current capability may be limited and other performance may vary from noted electrical characteristics when V<sub>OUT</sub> is not set to nominal.

<sup>[</sup>f] Refer to Output Ripple plots.

<sup>[</sup>g] Refer to Load Current vs. Ambient Temperature curves.

<sup>[</sup>h] Refer to Switching Frequency vs. Load current curves.

<sup>[</sup>i] Contact factory applications for array derating and layout best practices to minimize sharing errors.

<sup>[</sup>j] Informational only.

Parameter	Symbol	Conditions	Min	Тур	Max	Unit
		Timing				
Switching Frequency	f <sub>s</sub>	<sup>[h]</sup> While in DCM operating mode only, SYNCI grounded	470	500	530	kHz
Fault Restart Delay	t <sub>FR_DLY</sub>			30		ms
		Synchronization Input (SYNCI)				
Synchronization Frequency Range	f <sub>SYNCI</sub>	-50% and $+10%$ relative to set switching frequency (f <sub>s</sub> ), while in DCM operating mode only. <sup>[e]</sup> and <sup>[h]</sup>	250		550	kHz
SYNCI Threshold	V <sub>SYNCI</sub>			2.5		V
		Synchronization Output (SYNCO)				
SYNCO High	V <sub>SYNCO_HI</sub>	Source 1mA	4.5			V
SYNCO Low	V <sub>SYNCO_LO</sub>	Sink 1mA			0.5	V
SYNCO Rise Time	t <sub>SYNCO_RT</sub>	20pF load		10		ns
SYNCO Fall Time	t <sub>SYNCO_FT</sub>	20pF load		10		ns
		Soft Start, Tracking and Error Amplifier				
TRK Active Range (Nominal)	$V_{TRK}$		0		1.4	V
TRK Enable Threshold	V <sub>TRK_OV</sub>			40		mV
TRK to EAIN Offset	V <sub>EAIN_OV</sub>		40	80	120	mV
Charge Current (Soft Start)	I <sub>TRK</sub>		30	50	70	μΑ
Discharge Current (Fault)	I <sub>TRK_DIS</sub>	$V_{TRK} = 0.5V$		8.7		mA
TRK Capacitance, External	C <sub>TRK_EXT</sub>		47			nF
Soft Start Time	t <sub>SS</sub>	C <sub>TRK</sub> = 47nF		0.94		ms
Error Amplifier Transconductance	GM <sub>EAO</sub>	[d]		7.6		mS
PSM Skip Threshold	PSM <sub>SKIP</sub>	[d]		0.8		V
Error Amplifier Output Impedance	R <sub>OUT</sub>	[d]	1			MΩ
Internal Compensation Resistor	$R_{ZI}$	[d]		6		kΩ

<sup>[</sup>c] All parameters reflect regulator and inductor system performance. Measurements were made using a standard PI358x evaluation board with 3 x 3in dimensions and 4 layer, 2oz copper. Refer to inductor pairing table within Application Description section for specific inductor manufacturer and value.



<sup>[</sup>d] Regulator is assured to meet performance specifications by design, test correlation, characterization, and/or statistical process control. Output voltage is determined by an external feedback divider ratio.

<sup>[</sup>e] Output current capability may be limited and other performance may vary from noted electrical characteristics when V<sub>OUT</sub> is not set to nominal.

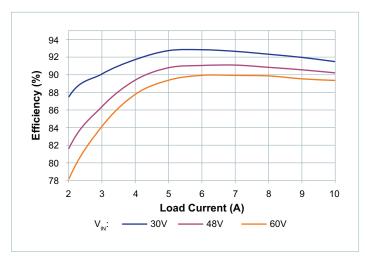
<sup>[</sup>f] Refer to Output Ripple plots.

<sup>[</sup>g] Refer to Load Current vs. Ambient Temperature curves.

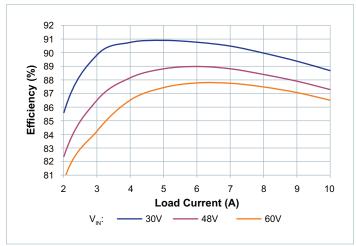
<sup>&</sup>lt;sup>[h]</sup> Refer to Switching Frequency vs. Load current curves.

<sup>[</sup>i] Contact factory applications for array derating and layout best practices to minimize sharing errors.

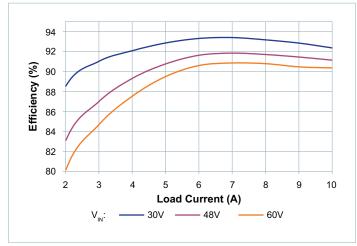
<sup>[</sup>j] Informational only.



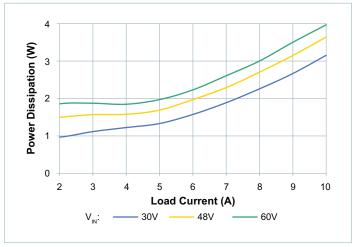
**Figure 1** — System efficiency, nominal trim, board temperature = 25°C



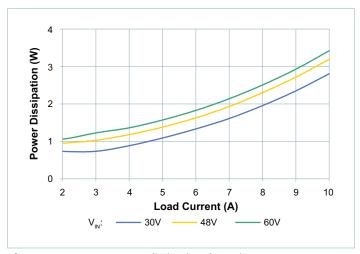
**Figure 2** — System efficiency, low trim, board temperature = 25°C



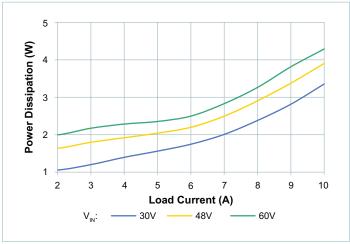
**Figure 3** — System efficiency, high trim, board temperature = 25°C



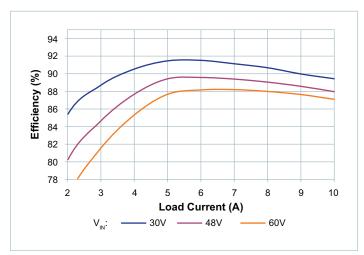
**Figure 4** — System power dissipation, nominal trim, board temperature = 25°C



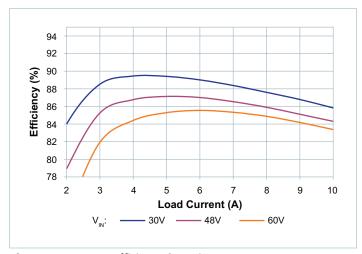
**Figure 5** — System power dissipation, low trim, board temperature = 25°C



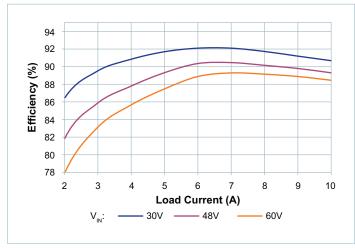
**Figure 6** — System power dissipation, high trim, board temperature = 25°C



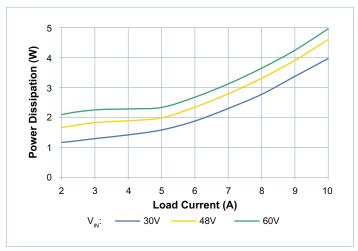
**Figure 7** — System efficiency, nominal trim, board temperature = 90°C



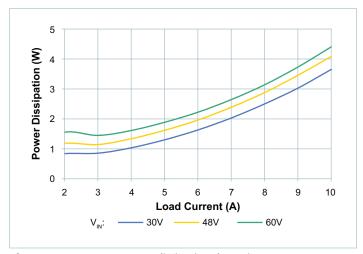
**Figure 8** — System efficiency, low trim, board temperature = 90°C



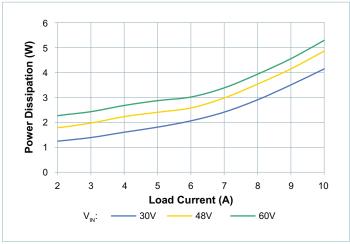
**Figure 9** — System efficiency, high trim, board temperature = 90°C



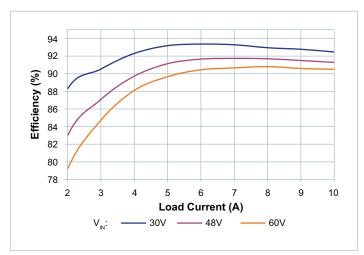
**Figure 10** — System power dissipation, nominal trim, board temperature = 90°C



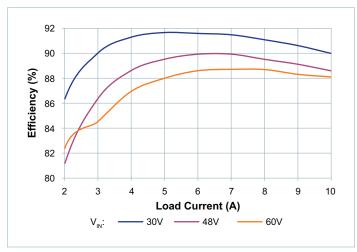
**Figure 11** — System power dissipation, low trim, board temperature = 90°C



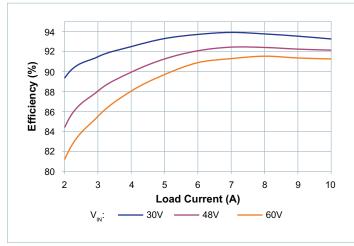
**Figure 12** — System power dissipation, high trim, board temperature = 90°C



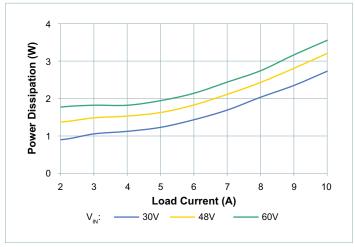
**Figure 13** — System efficiency, nominal trim, board temperature = −20°C



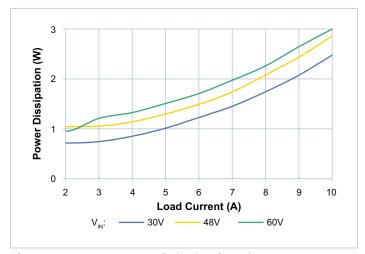
**Figure 14** — System efficiency, low trim, board temperature = -20°C



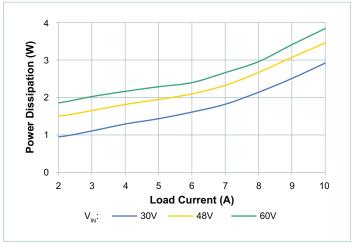
**Figure 15** — System efficiency, high trim, board temperature = -20°C



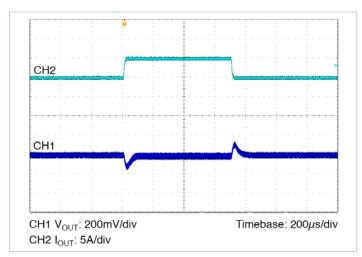
**Figure 16** — System power dissipation, nominal trim, board temperature = −20°C



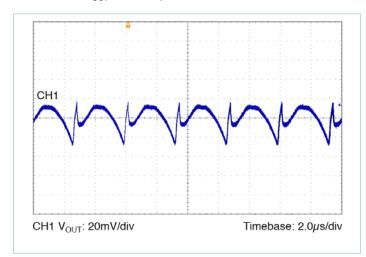
**Figure 17** — System power dissipation, low trim, board temperature = -20°C



**Figure 18** — System power dissipation, high trim, board temperature = -20°C



**Figure 19** — Transient response: 50% to 100% load, at 1A/ $\mu$ s; nominal line, nominal trim,  $C_{OUT} = 6 \times 100 \mu$ F ceramic



**Figure 20** — Output voltage ripple: nominal line, nominal trim, 100% load,  $C_{OUT} = 6 \times 100 \mu F$  ceramic, 20MHz BW

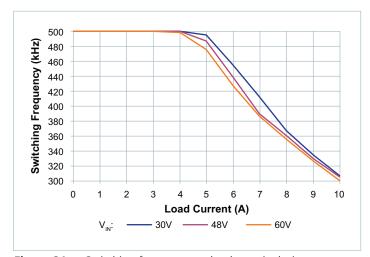


Figure 21 — Switching frequency vs. load, nominal trim

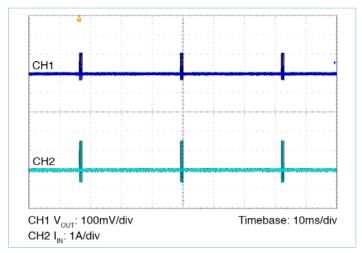
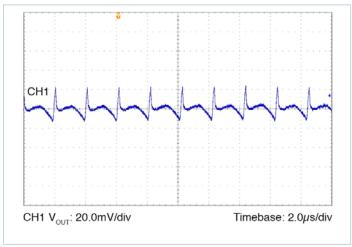
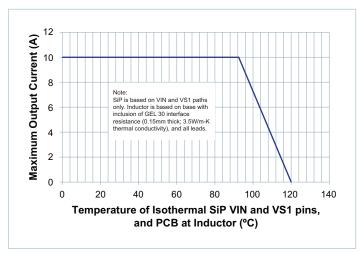


Figure 22 — Output short circuit, nominal line

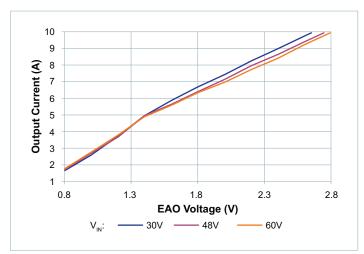


**Figure 23** — Output voltage ripple: nominal line, nominal trim, 50% load, C<sub>OUT</sub> = 6 x 100μF ceramic, 20MHz BW

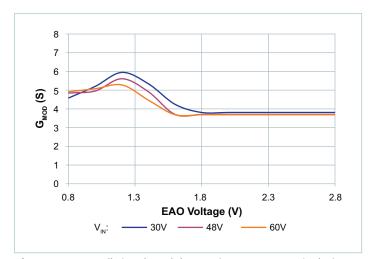


**Figure 24** — System thermal specified operating area: max I<sub>OUT</sub> at nominal trim vs. temperature at locations noted





**Figure 25** — Output current vs.  $V_{EAO}$ , nominal trim



**Figure 26** — Small-signal modulator gain vs.  $V_{EAO}$ , nominal trim

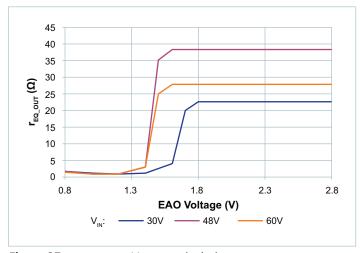


Figure 27 —  $r_{EQ\_OUT}$  vs  $V_{EAO}$ , nominal trim



Parameter	Symbol	Conditions	Min	Тур	Max	Unit
		Innut Considirations				
land the North and	\ \\	Input Specifications	20	40	60	1/
Input Voltage	V <sub>IN_DC</sub>	V 40) 4 T 2505 (	30	48	60	V
Input Current	I <sub>IN_DC</sub>	$V_{IN} = 48V$ , $T_{CASE} = 25$ °C, full load		1.12		А
Input Current at Output Short (Fault Condition Duty Cycle)	I <sub>IN_Short</sub>	Short at terminals		1.8		mA
Input Quiescent Current	$I_{Q_{-}VIN}$	Disabled		0.65		mA
Input Quiescent Current	I <sub>Q_VIN</sub>	Enabled, no load, T <sub>CASE</sub> = 25°C		2		mA
Input Voltage Slew Rate	V <sub>IN_SR</sub>				1	V/µs
		Output Specifications				
EAIN Voltage Total Regulation	V <sub>EAIN</sub>	[d]	0.975	0.990	1.005	V
Output Voltage Trim Range	V <sub>OUT DC</sub>	[d] [e]	3.8	5.0	6.5	V
Line Regulation	ΔV <sub>OUT</sub> / ΔV <sub>IN</sub>	@ 25°C, 30V < V <sub>IN</sub> < 60V		0.10		%
Load Regulation	ΔV <sub>OUT</sub> / ΔI <sub>OUT</sub>	@ 25°C, 10% to 100% load		0.10		%
Output Voltage Ripple	V <sub>OUT_AC</sub>	Full load, $C_{OUT} = 6 \times 47 \mu F$ , 20MHz BW <sup>[f]</sup>		60		mV <sub>P-P</sub>
Output Current	I <sub>OUT_DC</sub>	[9]	0		10	А
Current Limit	I <sub>OUT_CL</sub>	Typical current limit based on nominal 420nH inductor.		11.5		А
Maximum Array Size	N <sub>PARALLEL</sub>	[d]			3	Module
Output Current, Array of 2	I <sub>OUT_DC_ARRAY2</sub>	Total array capability, [d] see applications section for details	0		[i]	А
Output Current, Array of 3	I <sub>OUT_DC_ARRAY3</sub>	Total array capability, <sup>[d]</sup> see applications section for details	0		[i]	А
		Protection				
Input UVLO Start Threshold	V <sub>UVLO_START</sub>			27.0	29.1	V
Input UVLO Stop Hysteresis	V <sub>UVLO_HYS</sub>		1.66	2.08	2.50	V
Input UVLO Response Time				1.25		μs
Input OVLO Stop Threshold	V <sub>OVLO_STOP</sub>	[d]		64.3		V
Input OVLO Start Hysteresis	V <sub>OVLO_HYS</sub>	Hysteresis active when OVLO present for at least $t_{\text{FR\_DLY}}^{}$		1.17		V
Input OVLO Start Threshold	V <sub>OVLO_START</sub>	[d]	60.5			V
Input OVLO Response Time	t <sub>f</sub>			1.25		μs
Output Overvoltage Protection, Relative	V <sub>OVP_REL</sub>	Above set V <sub>OUT</sub>		20		%
Output Overvoltage Protection, Absolute	V <sub>OVP_ABS</sub>		6.7	7.5		V

<sup>[</sup>c] All parameters reflect regulator and inductor system performance. Measurements were made using a standard Pl358x evaluation board with 3 x 3in dimensions and 4 layer, 2oz copper. Refer to inductor pairing table within Application Description section for specific inductor manufacturer and value.



<sup>[</sup>d] Regulator is assured to meet performance specifications by design, test correlation, characterization, and/or statistical process control. Output voltage is determined by an external feedback divider ratio.

<sup>[</sup>e] Output current capability may be limited and other performance may vary from noted electrical characteristics when V<sub>OUT</sub> is not set to nominal.

<sup>[</sup>f] Refer to Output Ripple plots.

<sup>[</sup>g] Refer to Load Current vs. Ambient Temperature curves.

<sup>[</sup>h] Refer to Switching Frequency vs. Load current curves.

<sup>[</sup>i] Contact factory applications for array derating and layout best practices to minimize sharing errors.

<sup>[</sup>j] Informational only.

Parameter	Symbol	Conditions	Min	Тур	Max	Unit			
Timing									
Switching Frequency	f <sub>s</sub>	[h] While in DCM operating mode only, SYNCI grounded	564	600	636	kHz			
Fault Restart Delay	t <sub>FR_DLY</sub>			30		ms			
		Synchronization Input (SYNCI)							
Synchronization Frequency Range	f <sub>SYNCI</sub>	-50% and +10% relative to set switching frequency (f <sub>s</sub> ), while in DCM operating mode only. <sup>[e]</sup> and <sup>[h]</sup>	300		660	kHz			
SYNCI Threshold	V <sub>SYNCI</sub>			2.5		V			
		Synchronization Output (SYNCO)							
SYNCO High	V <sub>SYNCO_HI</sub>	Source 1mA	4.5			V			
SYNCO Low	V <sub>SYNCO_LO</sub>	Sink 1mA			0.5	V			
SYNCO Rise Time	t <sub>SYNCO_RT</sub>	20pF load		10		ns			
SYNCO Fall Time	t <sub>SYNCO_FT</sub>	20pF load		10		ns			
		Soft Start, Tracking and Error Amplifier							
TRK Active Range (Nominal)	$V_{TRK}$		0		1.4	V			
TRK Enable Threshold	V <sub>TRK_OV</sub>			40		mV			
TRK to EAIN Offset	V <sub>EAIN_OV</sub>		40	80	120	mV			
Charge Current (Soft Start)	I <sub>TRK</sub>		30	50	70	μΑ			
Discharge Current (Fault)	I <sub>TRK_DIS</sub>	$V_{TRK} = 0.5V$		8.7		mA			
TRK Capacitance, External	C <sub>TRK_EXT</sub>		47			nF			
Soft Start Time	t <sub>SS</sub>	C <sub>TRK</sub> = 47nF		0.94		ms			
Error Amplifier Transconductance	GM <sub>EAO</sub>	[d]		7.6		mS			
PSM Skip Threshold	PSM <sub>SKIP</sub>	[d]		0.8		V			
Error Amplifier Output Impedance	R <sub>OUT</sub>	[d]	1			MΩ			
Internal Compensation Resistor	$R_{ZI}$	[d]		6		kΩ			

<sup>[</sup>c] All parameters reflect regulator and inductor system performance. Measurements were made using a standard PI358x evaluation board with 3 x 3in dimensions and 4 layer, 2oz copper. Refer to inductor pairing table within Application Description section for specific inductor manufacturer and value.



<sup>[</sup>d] Regulator is assured to meet performance specifications by design, test correlation, characterization, and/or statistical process control. Output voltage is determined by an external feedback divider ratio.

<sup>[</sup>e] Output current capability may be limited and other performance may vary from noted electrical characteristics when V<sub>OUT</sub> is not set to nominal.

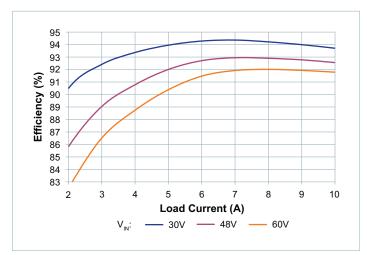
<sup>[</sup>f] Refer to Output Ripple plots.

<sup>[</sup>g] Refer to Load Current vs. Ambient Temperature curves.

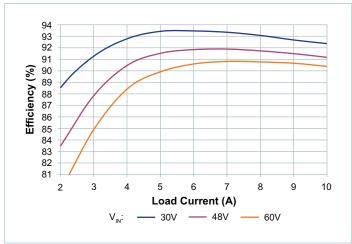
<sup>&</sup>lt;sup>[h]</sup> Refer to Switching Frequency vs. Load current curves.

<sup>[</sup>i] Contact factory applications for array derating and layout best practices to minimize sharing errors.

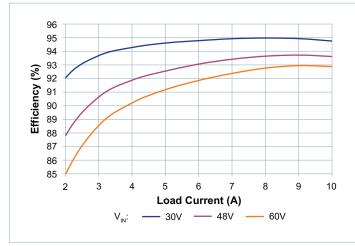
<sup>[</sup>j] Informational only.



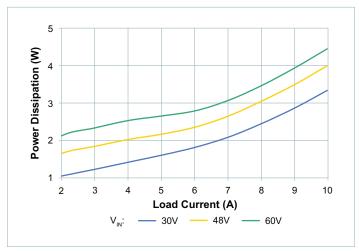
**Figure 28** — System efficiency, nominal trim, board temperature = 25°C



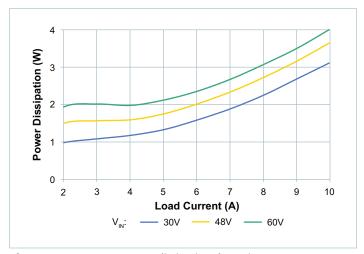
**Figure 29** — System efficiency, low trim, board temperature = 25°C



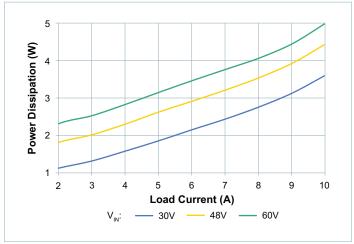
**Figure 30** — System efficiency, high trim, board temperature = 25°C



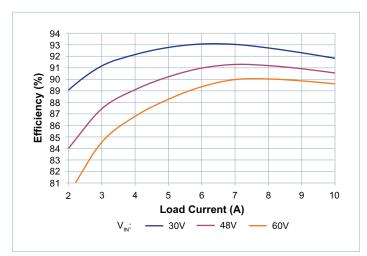
**Figure 31** — System power dissipation, nominal trim, board temperature = 25°C



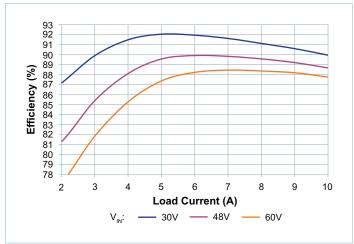
**Figure 32** — System power dissipation, low trim, board temperature = 25°C



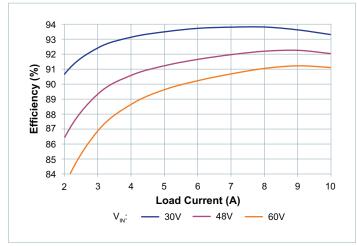
**Figure 33** — System power dissipation, high trim, board temperature = 25°C



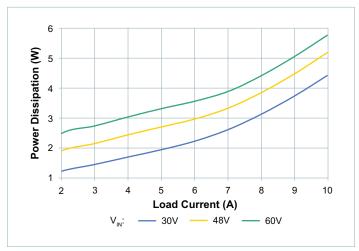
**Figure 34** — System efficiency, nominal trim, board temperature = 90°C



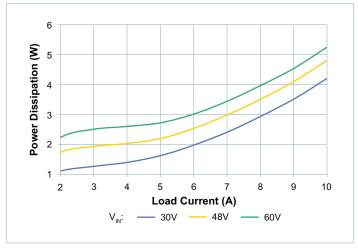
**Figure 35** — System efficiency, low Trim, board temperature = 90°C



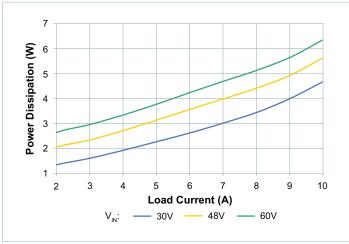
**Figure 36** — System efficiency, high trim, board temperature = 90°C



**Figure 37** — System power dissipation, nominal trim, board temperature = 90°C

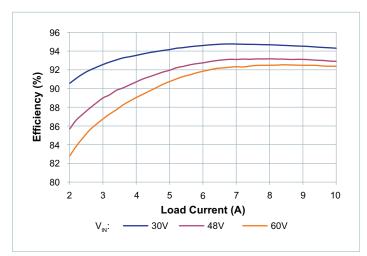


**Figure 38** — System power dissipation, low trim, board temperature = 90°C

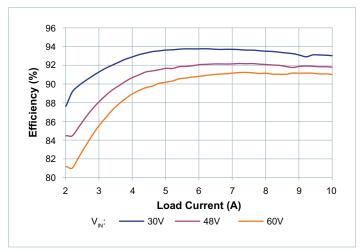


**Figure 39** — System power dissipation, high trim, board temperature = 90°C

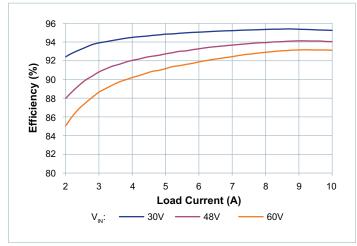




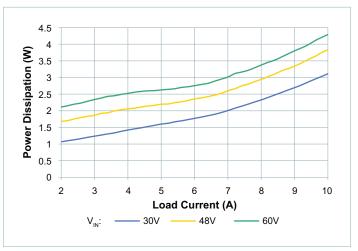
**Figure 40** — System efficiency, nominal trim, board temperature = −20°C



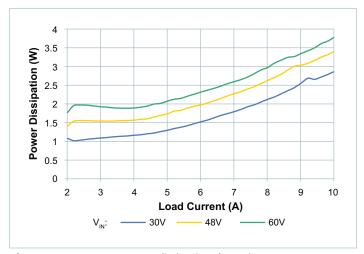
**Figure 41** — System efficiency, low trim, board temperature = -20°C



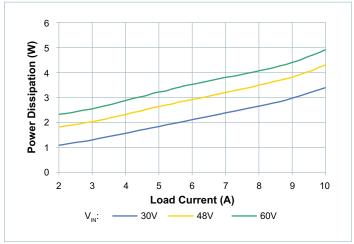
**Figure 42** — System efficiency, high trim, board temperature = -20°C



**Figure 43** — System power dissipation, nominal trim, board temperature = −20°C

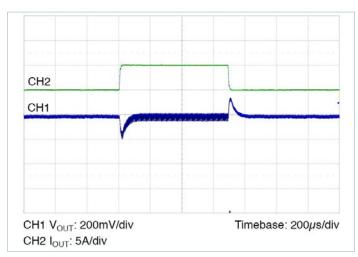


**Figure 44** — System power dissipation, low trim, board temperature = -20°C

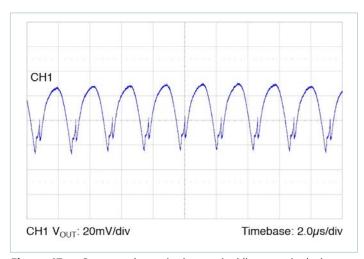


**Figure 45** — System power dissipation, high trim, board temperature = -20°C





**Figure 46** — Transient response: 50% to 100% load, at 1A/µs; nominal line, nominal trim,  $C_{OUT} = 6 \times 47 \mu F \text{ ceramic}$ 



**Figure 47** — Output voltage ripple: nominal line, nominal trim, 100% load,  $C_{OUT} = 6 \times 47 \mu F$  ceramic, 20MHz BW

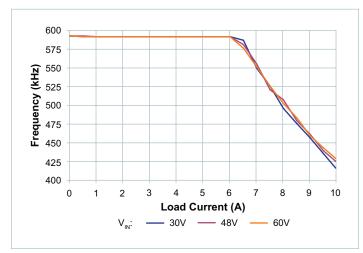


Figure 48 — Switching frequency vs. load, nominal trim

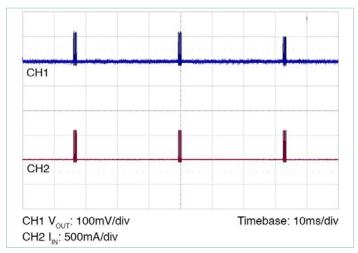
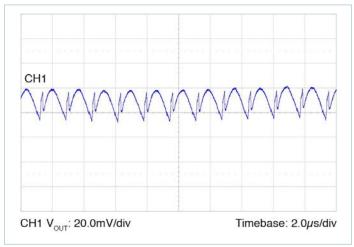
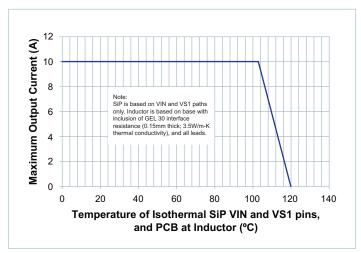


Figure 49 — Output short circuit, nominal line

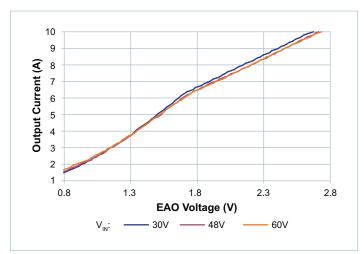


**Figure 50** — Output voltage ripple: nominal line, nominal trim, 50% load, C<sub>OUT</sub> = 6 x 47µF ceramic, 20MHz BW

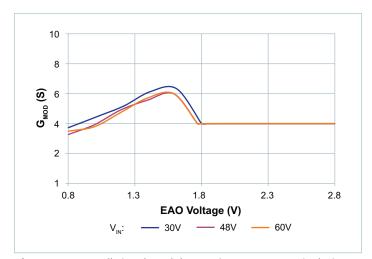


**Figure 51** — System thermal specified operating area: max I<sub>OUT</sub> at nominal trim vs. temperature at locations noted





**Figure 52** — Output current vs.  $V_{EAO}$ , nominal trim



**Figure 53** — Small-signal modulator gain vs.  $V_{EAO}$ , nominal trim

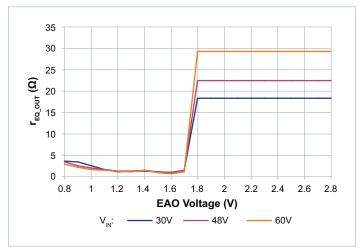


Figure 54 —  $r_{EQ\_OUT}$  vs  $V_{EAO}$ , nominal trim



Parameter	Symbol	Symbol Conditions		Тур	Max	Unit
		Input Specifications		I		
Input Voltage	V <sub>IN_DC</sub>		30	48	60	V
Input Current	I <sub>IN_DC</sub>	V <sub>IN</sub> = 48V, T <sub>CASE</sub> = 25°C, full load		2.35		А
Input Current at Output Short (Fault Condition Duty Cycle)	I <sub>IN_Short</sub>	Short at terminals		3.5		mA
Input Quiescent Current	I <sub>Q_VIN</sub>	Disabled		0.65		mA
Input Quiescent Current	I <sub>Q_VIN</sub>	Enabled, no load, T <sub>CASE</sub> = 25°C		3		mA
Input Voltage Slew Rate	V <sub>IN_SR</sub>				1	V/µs
		Output Specifications				
EAIN Voltage Total Regulation	V <sub>EAIN</sub>	[d]	0.975	0.990	1.005	V
Output Voltage Trim Range	V <sub>OUT_DC</sub>	[d] [e]	6.5	12.0	14.0	V
Line Regulation	ΔV <sub>OUT</sub> / ΔV <sub>IN</sub>	@ 25°C, 30V < V <sub>IN</sub> < 60V	0.5	0.1		%
Load Regulation	ΔV <sub>OUT</sub> / ΔI <sub>OUT</sub>	@ 25°C, 10% to 100% load		0.1		%
Output Voltage Ripple	V <sub>OUT AC</sub>	Full load, C <sub>OUT</sub> = 6 x 10µF, 20MHz BW <sup>[f]</sup>		115		mV <sub>P-P</sub>
Output Current	I <sub>OUT DC</sub>	[9]	0		9	А
Current Limit	I <sub>OUT CL</sub>	Typical current limit based on nominal 900nH inductor		10.5		А
Maximum Array Size	N <sub>PARALLEL</sub>	[d]			3	Modules
Output Current, Array of 2	I <sub>OUT_DC_ARRAY2</sub>	Total array capability, [d] see applications section for details	0		[i]	А
Output Current, Array of 3	I <sub>OUT_DC_ARRAY3</sub>	Total array capability, <sup>[d]</sup> see applications section for details	0		[i]	А
		Protection				
Input UVLO Start Threshold	V <sub>UVLO_START</sub>			27.0	29.1	V
Input UVLO Stop Hysteresis	V <sub>UVLO_HYS</sub>		1.66	2.08	2.50	V
Input UVLO Response Time				1.25		μs
Input OVLO Stop Threshold	V <sub>OVLO_STOP</sub>	[d]		64.3		V
Input OVLO Start Hysteresis	V <sub>OVLO_HYS</sub>	Hysteresis active when OVLO present for at least $t_{\text{FR\_DLY}}^{\text{[d]}}$		1.17		V
Input OVLO Start Threshold	V <sub>OVLO_START</sub>	[d]	60.5			V
Input OVLO Response Time	t <sub>f</sub>			1.25		μs
Output Overvoltage Protection, Relative	V <sub>OVP_REL</sub>	Above set V <sub>OUT</sub>		20		%
Output Overvoltage Protection, Absolute	V <sub>OVP_ABS</sub>		14.7	15.8		V

<sup>[</sup>c] All parameters reflect regulator and inductor system performance. Measurements were made using a standard Pl358x evaluation board with 3 x 3in dimensions and 4 layer, 2oz copper. Refer to inductor pairing table within Application Description section for specific inductor manufacturer and value.



<sup>[</sup>d] Regulator is assured to meet performance specifications by design, test correlation, characterization, and/or statistical process control. Output voltage is determined by an external feedback divider ratio.

<sup>[</sup>e] Output current capability may be limited and other performance may vary from noted electrical characteristics when V<sub>OUT</sub> is not set to nominal.

<sup>[</sup>f] Refer to Output Ripple plots.

<sup>[</sup>g] Refer to Load Current vs. Ambient Temperature curves.

<sup>[</sup>h] Refer to Switching Frequency vs. Load current curves.

<sup>[</sup>i] Contact factory applications for array derating and layout best practices to minimize sharing errors.

<sup>[</sup>j] Informational only.

Parameter	Symbol	Conditions	Min	Тур	Max	Unit			
Timing									
Switching Frequency	f <sub>s</sub>	<sup>[h]</sup> While in DCM operating mode only, SYNCI grounded	658	700	742	kHz			
Fault Restart Delay	t <sub>FR_DLY</sub>			30		ms			
		Synchronization Input (SYNCI)							
Synchronization Frequency Range	f <sub>SYNCI</sub>	-50% and $+10%$ relative to set switching frequency (f <sub>S</sub> ), while in DCM operating mode only. <sup>[e]</sup> and <sup>[h]</sup>	350		770	kHz			
SYNCI Threshold	V <sub>SYNCI</sub>			2.5		V			
		Synchronization Output (SYNCO)							
SYNCO High	V <sub>SYNCO_HI</sub>	Source 1mA	4.5			V			
SYNCO Low	V <sub>SYNCO_LO</sub>	Sink 1mA			0.5	V			
SYNCO Rise Time	t <sub>SYNCO_RT</sub>	20pF load		10		ns			
SYNCO Fall Time	t <sub>SYNCO_FT</sub>	20pF load		10		ns			
		Soft Start, Tracking and Error Amplifier							
TRK Active Range (Nominal)	$V_{TRK}$		0		1.4	V			
TRK Enable Threshold	V <sub>TRK_OV</sub>			40		mV			
TRK to EAIN Offset	V <sub>EAIN_OV</sub>		40	80	120	mV			
Charge Current (Soft Start)	I <sub>TRK</sub>		30	50	70	μΑ			
Discharge Current (Fault)	I <sub>TRK_DIS</sub>	$V_{TRK} = 0.5V$		8.7		mA			
TRK Capacitance, External	C <sub>TRK_EXT</sub>		47			nF			
Soft Start Time	t <sub>SS</sub>	C <sub>TRK</sub> = 47nF		0.94		ms			
Error Amplifier Transconductance	GM <sub>EAO</sub>	[d]		7.6		mS			
PSM Skip Threshold	PSM <sub>SKIP</sub>	[d]		0.8		V			
Error Amplifier Output Impedance	R <sub>OUT</sub>	[d]	1			MΩ			
Internal Compensation Resistor	R <sub>ZI</sub>	[d]		6		kΩ			

<sup>[</sup>c] All parameters reflect regulator and inductor system performance. Measurements were made using a standard PI358x evaluation board with 3 x 3in dimensions and 4 layer, 2oz copper. Refer to inductor pairing table within Application Description section for specific inductor manufacturer and value.



<sup>[</sup>d] Regulator is assured to meet performance specifications by design, test correlation, characterization, and/or statistical process control. Output voltage is determined by an external feedback divider ratio.

<sup>[</sup>e] Output current capability may be limited and other performance may vary from noted electrical characteristics when V<sub>OUT</sub> is not set to nominal.

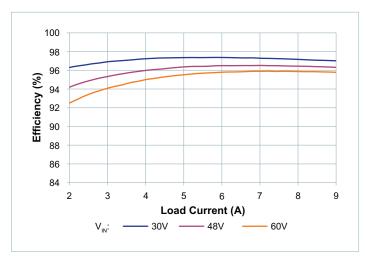
<sup>[</sup>f] Refer to Output Ripple plots.

<sup>[</sup>g] Refer to Load Current vs. Ambient Temperature curves.

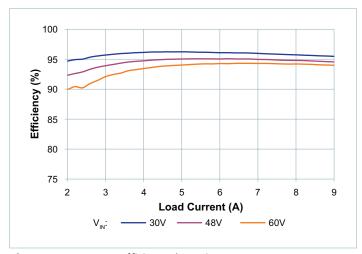
<sup>&</sup>lt;sup>[h]</sup> Refer to Switching Frequency vs. Load current curves.

<sup>[</sup>i] Contact factory applications for array derating and layout best practices to minimize sharing errors.

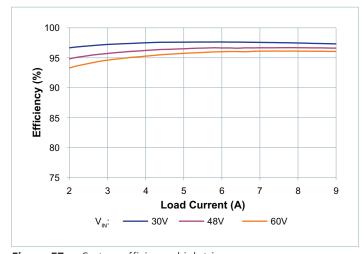
<sup>[</sup>j] Informational only.



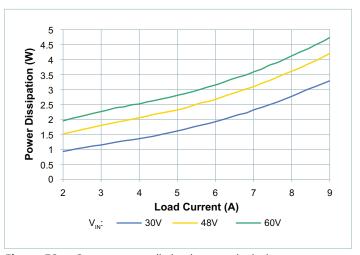
**Figure 55** — System efficiency, nominal trim, board temperature = 25°C



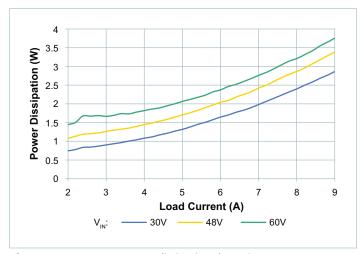
**Figure 56** — System efficiency, low trim, board temperature = 25°C



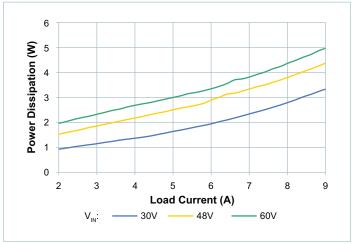
**Figure 57** — System efficiency, high trim, board temperature = 25°C



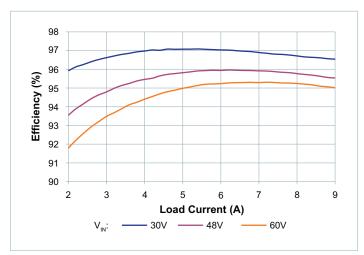
**Figure 58** — System power dissipation, nominal trim, board temperature = 25°C



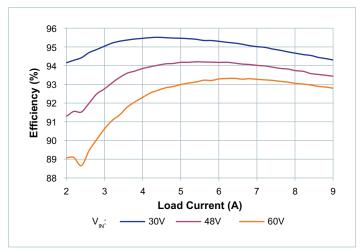
**Figure 59** — System power dissipation, low trim, board temperature = 25°C



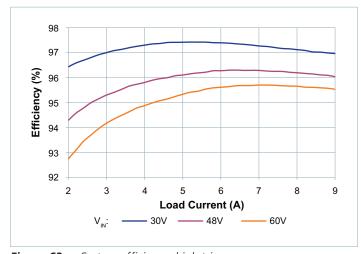
**Figure 60** — System power dissipation, high trim, board temperature = 25°C



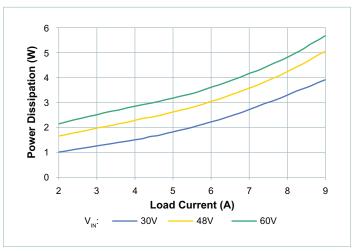
**Figure 61** — System efficiency, nominal trim, board temperature = 90°C



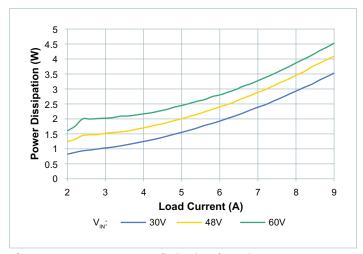
**Figure 62** — System efficiency, low Trim, board temperature = 90°C



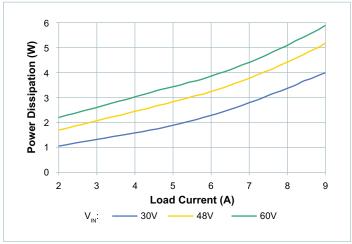
**Figure 63** — System efficiency, high trim, board temperature = 90°C



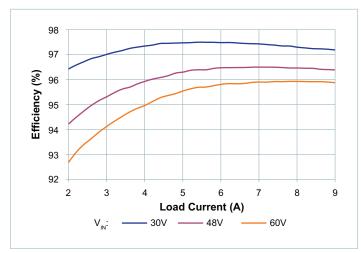
**Figure 64** — System power dissipation, nominal trim, board temperature = 90°C



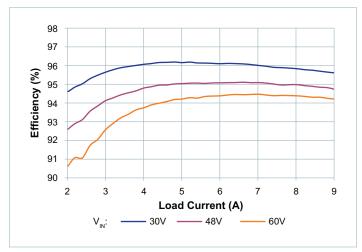
**Figure 65** — System power dissipation, low trim, board temperature = 90°C



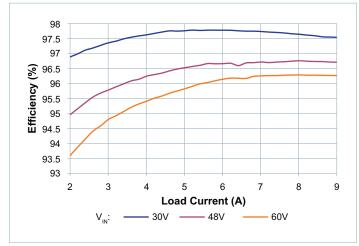
**Figure 66** — System power dissipation, high trim, board temperature = 90°C



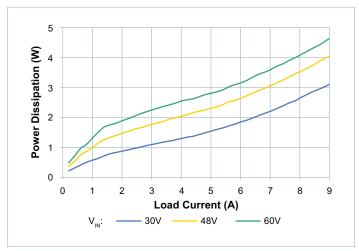
**Figure 67** — System efficiency, nominal trim, board temperature =  $-20^{\circ}$ C



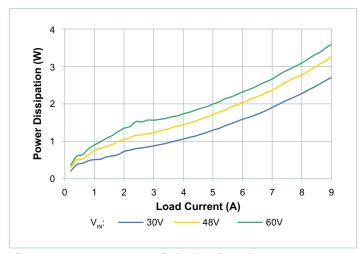
**Figure 68** — System efficiency, low trim, board temperature = -20°C



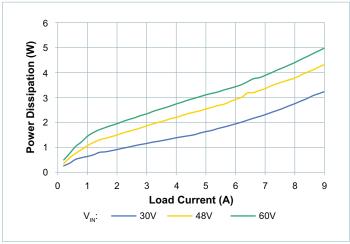
**Figure 69** — System efficiency, high trim, board temperature = -20°C



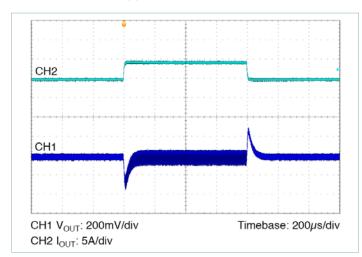
**Figure 70** — System power dissipation, nominal trim, board temperature = −20°C



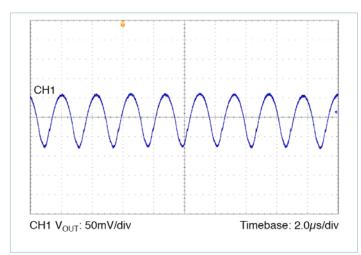
**Figure 71** — System power dissipation, low trim, board temperature = −20°C



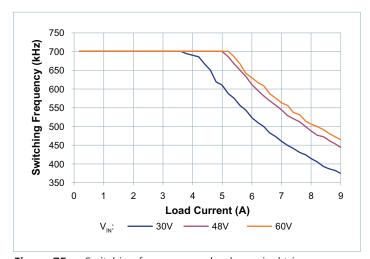
**Figure 72** — System power dissipation, high trim, board temperature = -20°C



**Figure 73** — Transient response: 50% to 100% load, at 1A/µs; nominal line, nominal trim,  $C_{OUT} = 6 \times 47 \mu F \text{ ceramic}$ 



**Figure 74** — Output voltage ripple: nominal line, nominal trim, 100% load,  $C_{OUT} = 6 \times 47 \mu F$  ceramic, 20MHz BW



**Figure 75** — Switching frequency vs. load, nominal trim

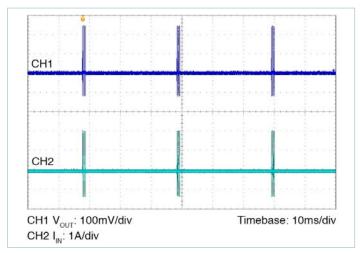
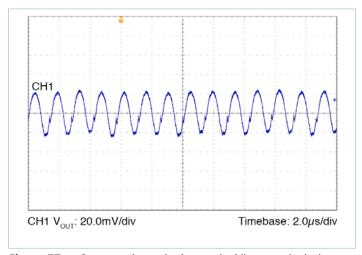
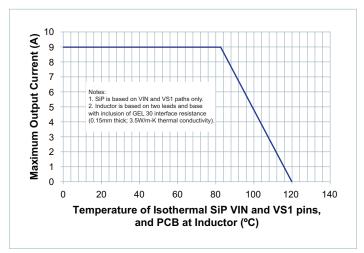


Figure 76 — Output short circuit, nominal line

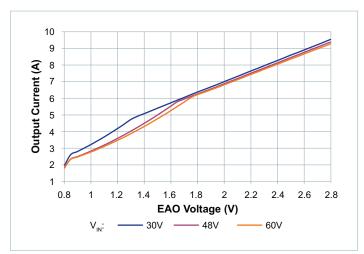


**Figure 77** — Output voltage ripple: nominal line, nominal trim, 50% load,  $C_{OUT} = 6 \times 47 \mu F$  ceramic, 20MHz BW



**Figure 78** — System thermal specified operating area: max I<sub>OUT</sub> at nominal trim vs. temperature at locations noted

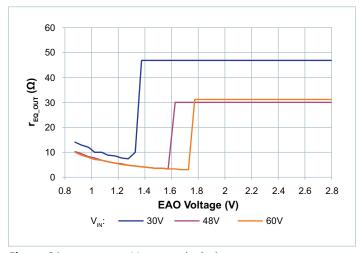




**Figure 79** — Output current vs.  $V_{EAO}$ , nominal trim



**Figure 80** — Small-signal modulator gain vs.  $V_{EAO}$ , nominal trim



**Figure 81** —  $r_{EQ\_OUT}$  vs  $V_{EAO}$ , nominal trim



## **Functional Description**

The PI358x-00 is a family of highly integrated ZVS Buck regulators. The PI358x-00 has an output voltage that can be set within a prescribed range. Performance and maximum output current are characterized with a specific external power inductor (see Table 4).

For basic operation, Figure 82 shows the connections and components required. No additional design or settings are required.

If the exact recommended part cannot be used, the description column of Table 1 serves as a guidance for an alternate part. Any substitute parts should be equal to or better than the original for all parameters.

Reasonable engineering judgment in making the choices for alternative components and a detailed verification of the performance would be highly recommended.

#### **ENABLE (EN)**

EN is the enable pin of the converter. The EN pin is referenced to SGND and permits the user to turn the regulator on or off. The EN default polarity is a positive logic assertion. If the EN pin is left floating or asserted high, the converter output is enabled. Pulling EN pin below  $V_{\text{EN\_LO}}$  with respect to SGND will disable the regulator output.

## **Remote Sensing**

If remote sensing is required, the PI358x-00 product family is equipped with a general purpose op-amp. This amplifier can allow full differential remote sense by configuring it as a differential follower and connecting the  $V_{\rm DIFF}$  pin to the EAIN pin.



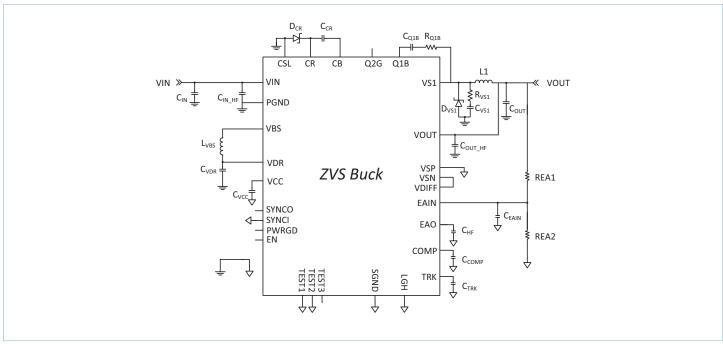


Figure 82 — ZVS Buck with required components

Reference Designation	Manufacturer	Part Number	Value	Description				
C <sub>OUT</sub>	Refer to Table 6 – Re	Refer to Table 6 – Recommended input and output capacitor components						
C <sub>OUT_HF</sub>	Murata	Murata GRM21BR72A474KA73K 0.47μF Capacitor, X7R Ceramic, 0.47μF, 100V, 10						
C <sub>IN_HF</sub>	Murata	GRM21BR72A474KA73K	0.47µF	Capacitor, X7R Ceramic, 0.47µF, 100V, 10%, 0805				
C <sub>Q1B</sub>	TDK	C1608X7R1C224K080AC	0.22µF	Capacitor, X7R, 0.22µF, 16V, 10%, 0603				
R <sub>Q1B</sub>	Rohm	ESR03EZPJ1R3	1.3Ω	RES SMD 1.3Ω 5% 1/4W 0603				
D <sub>CR</sub>	Nexperia	PMEG4002EL		Diode, Schottky, PMEG4002EL Philips, 40V, 200mA, SOD882				
C <sub>CR</sub>	Murata	GCM188R71H473KA55D	47nF	Capacitor, Ceramic, 47nF, 50V, 0603				
D <sub>VS1</sub>	Nexperia	PMEG10010ELR		Diode, Schottky, 100V, 1A, low V <sub>F</sub> , low leakage current, SOD123W				
C <sub>VS1</sub>	TDK	C1608C0G2A102J080AA	1nF	Capacitor, C0G, 100V, 1nF, 5%, 0603				
R <sub>VS1</sub>	Samsung	RUT1608FR300CS	0.3Ω	RES SMD 300mΩ 1%1/8W 0603				
L <sub>VBS</sub>	TDK	MLZ2012M100HT	10µH	Inductor, 10µH ±20%, 300mA, 2Mhz, 0805				
C <sub>VDR</sub> , C <sub>VCC</sub>	Murata	GRM188R71A225KE15D	2.2µF	Capacitor, X7R Ceramic, 2.2µF, 10V, 0603				
C <sub>EAIN</sub>	56pF							
C <sub>COMP</sub>	4.7nF							
C <sub>HF</sub>	56pF							
C <sub>TRK</sub>	47nF							
L1	Refer to Inductor Pa	iring						
REA1	Defeate Application	Description for Output Valtage Cot Boilet						
REA2	kerer to Application	tefer to Application Description for Output Voltage Set Point						

**Table 1** — List of recommended components

#### **Soft Start**

The PI358x-00 requires an external soft-start capacitor from the TRK pin to SGND to control the rate of rise of the output voltage. Increasing the capacitance of this soft-start capacitor will increase the start-up ramp period. See, "Soft Start Adjustment and Track," in the Applications Description section for more details.

#### **Output Voltage Selection**

The PI358x-00 output voltage can be set with REA1 and REA2 as shown in Figure 82. Table 2 defines the allowable operational voltage ranges for the PI358x-00 family. Refer to the Output Voltage Set Point Application Description for details.

Device	Output Voltage				
Device	Nominal	Range			
PI3583-00-QFYZ	3.3V	2.2 – 4.0V			
PI3585-00-QFYZ	5.0V	3.8 – 6.5V			
PI3586-00-QFYZ	12.0V	6.5 – 14V			

Table 2 — PI358x-00 family output voltage ranges

#### **Output Current Limit Protection**

The PI358x-00 has a current limit protection, which prevents the output from sourcing current higher than the regulator's maximum rated current. If the output current exceeds the Current Limit ( $I_{OUT\_CL}$ ) for 1024µs, a slow current limit fault is initiated and the regulator is shutdown which eliminates output current flow. After Fault Restart Delay ( $t_{FR\_DLY}$ ), a soft-start cycle is initiated. This restart cycle will be repeated indefinitely until the excessive load is removed.

The PI358x-00 also has short circuit protection which can rapidly stop switching to protect against catastrophic failure of an external component such as a saturated inductor. If short circuit protection is triggered the PI358x-00 will complete the current cycle and stop switching. The module will attempt to soft start after Fault Restart Delay ( $t_{\text{FR}}$  DLY).

#### Input Undervoltage Lockout

If  $V_{\rm IN}$  falls below the input Undervoltage Lockout (UVLO) threshold, but remains high enough to power the bias supply, the PI358x-00 will complete the current cycle and stop switching. The system will soft start once the input voltage is reestablished and after the Fault Restart Delay.

#### **Input Overvoltage Lockout**

If  $V_{IN}$  exceeds the input Overvoltage Lockout (OVLO) threshold ( $V_{OVLO}$ ), while the controller is running, the PI358x-00 will complete the current cycle and stop switching. If  $V_{IN}$  remains above OVLO for at least  $t_{FR\_DLY}$ , then the input voltage is considered reestablished once  $V_{IN}$  goes below  $V_{OVLO}$ - $V_{OVLO\_HYS}$ . If  $V_{IN}$  goes below OVLO before  $t_{FR\_DLY}$  elapses, then the input voltage is considered reestablished once  $V_{IN}$  goes below  $V_{OVLO}$ . The system will soft start once the input voltage is reestablished and after the Fault Restart Delay.

#### **Output Overvoltage Protection**

The PI358x-00 family is equipped with output Overvoltage Protection (OVP) to prevent damage to input voltage sensitive devices. If the output voltage exceeds  $V_{\text{OVP-REL}}$  or  $V_{\text{OVP-ABS}}$ , the regulator will complete the current cycle and stop switching. The system will resume operation once the output voltage falls below the OVP threshold and after Fault Restart Delay.

#### **Overtemperature Protection**

The PI358x features an over temperature protection (OTP), which will not engage until after the product is operated above the maximum rated temperature. The OTP circuit is only designed to protect against catastrophic failure due to excessive temperatures and should not be relied upon to ensure the device stays within the recommended operating temperature range. Thermal shutdown terminates switching and discharges the soft-start capacitor. The PI358x will restart after the excessive temperature decreases by 30°C.

#### Pulse Skip Mode (PSM)

PI358x-00 features a Pulse Skip Mode (PSM) to achieve high efficiency at light loads. The regulators are setup to skip pulses if EAO falls below a PSM threshold (PSM $_{\rm SKIP}$ ). Depending on conditions and component values, this may result in single pulses or several consecutive pulses followed by skipped pulses. Skipping cycles significantly reduces gate drive power and improves light load efficiency. The regulator will leave PSM once the EAO rises above the Pulse Skip Mode threshold.

#### **Variable Frequency Operation**

Each PI358x-00 is preprogrammed to a base operating frequency, with respect to the power stage inductor (see Table 3), to operate at peak efficiency across line and load variations. At higher loads, the base operating frequency will decrease to accommodate storage of more energy in the main inductor. By increasing the switching period, ZVS operation is preserved throughout the total input line and output trim voltage ranges, maintaining optimum efficiency. The ZVS operation is preserved throughout the total input line voltage range therefore maintaining optimum efficiency.

#### **Thermal Characteristics**

Figure 83(a) and 83(c) thermal impedance models that can predict the maximum temperature of the hottest component for a given operating condition. This model assumes that all customer PCB connections are at one temperature, which is PCB equivalent Temperature  $T_{PCB}$  °C.

The SiP model can be simplified as shown in Figure 83(b). which assumes all PCB nodes are at the same temperature.



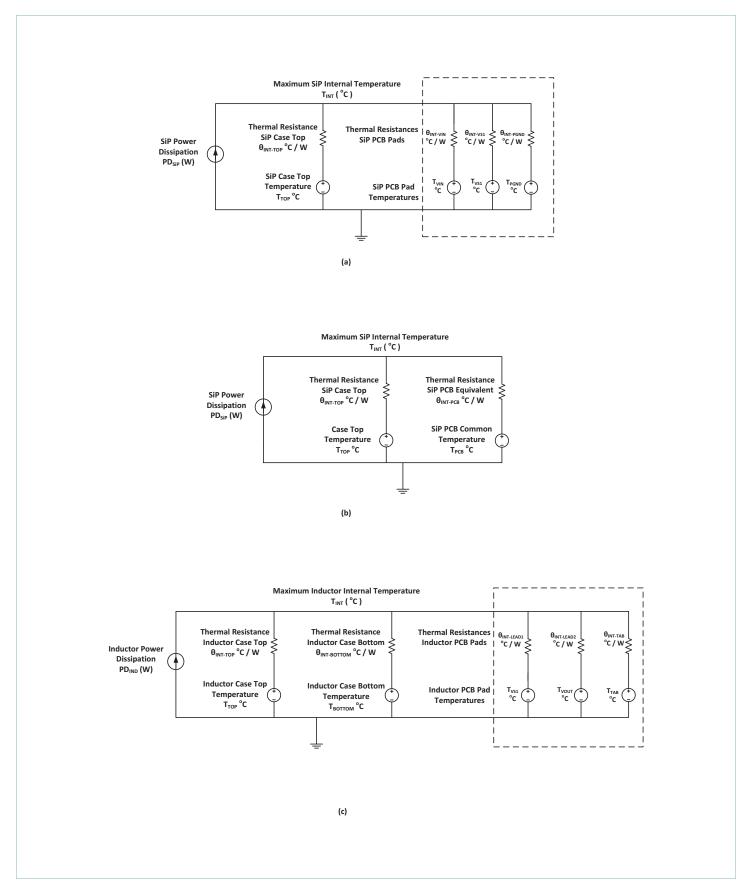


Figure 83 — Pl358x-00 thermal model (a), SiP simplified version (b) and inductor thermal model (c)

## Where the symbol in Figure 83(a) and (b) is defined as the following:

$\theta_{INT-TOP}$	the thermal impedance from the hottest component inside the SiP to the top side
$\theta_{INT-PCB}$	the thermal impedance from the hottest component inside the SiP to the customer PCB, assuming all pins are at one temperature.
θ <sub>INT-VIN</sub>	the thermal impedance from the hottest component inside the SiP to the circuit board VIN pads.
θ <sub>INT-VS1</sub>	the thermal impedance from the hottest component inside the SiP to the circuit board VS1 pads.
$\theta_{INT-PGND}$	the thermal impedance from the hottest component inside the SiP to the circuit board for PGND pin 1 and pin 37 combined.

## Where the symbol in Figure 83(c) is defined as the following:

$\theta_{INT-TOP}$	the thermal impedance from the hot spot to the top surface of the core.
$\theta_{INT-BOT}$	the thermal impedance from the hot spot to the bottom surface of the core.
$\theta_{INT-TAB}$	the thermal impedance from the hot spot to the metal mounting tab on the core body.
$\theta_{INT\text{-LEAD1}}$	the thermal impedance from the hot spot to one of the mounting leads. Since the leads are the same thermal impedance, there is no need to specify by explicit pin number.
$\theta_{INT\text{-LEAD2}}$	the thermal impedance from the hot spot to the other mounting lead.

The following equation can predict the junction temperature based on the heat load applied to the SiP and the known ambient conditions with the simplified thermal circuit model:

$$T_{INT} = \frac{PD + \frac{T_{TOP}}{\theta_{INT-TOP}} + \frac{T_{PCB}}{\theta_{INT-PCB}}}{\frac{1}{\theta_{INT-TOP}} + \frac{1}{\theta_{INT-PCB}}}$$
(1)



## Thermal Characteristics (Cont.)

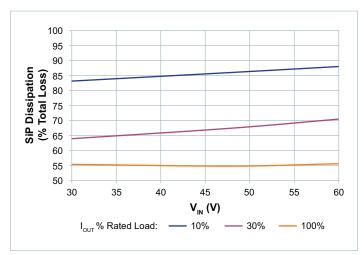
Product		ied SiP npedances	Detailed SiP Thermal Impedances				
System	θ <sub>INT-TOP</sub> (°C / W)	θ <sub>INT-PCB</sub> (°C / W)	θ <sub>INT-TOP</sub> (°C / W)	θ <sub>INT-VIN</sub> (°C / W)	θ <sub>INT-VS1</sub> (°C / W)	θ <sub>INT-PGND</sub> (°C / W)	
PI3583-00	44	0.53	44	1.4	0.95	7.7	
PI3585-00	54	0.64	54	2.6	0.92	9.6	
PI3586-00	29	0.42	29	0.88	1.2	2.2	

**Table 3** — PI358x-00 SiP thermal impedance

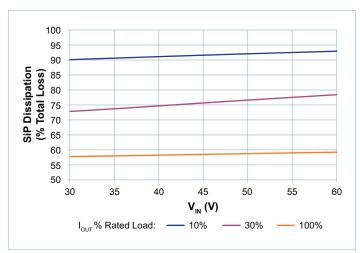
Product	Inductor Part	Thermal Impedances					
System	Number	θ <sub>INT-TOP</sub> (°C / W)	$\theta_{\text{INT-LEAD1}}$ , $\theta_{\text{INT-LEAD2}}$ (°C / W)	θ <sub>INT-BOTTOM</sub> (°C / W)	<sup>θ</sup> INT-TAB (°C / W)		
PI3583-00	HCV1206-R42-R	68	58	16	180		
PI3585-00	HCV1206-R42-R	110	58	21	140		
PI3586-00	HCV1206-R90-R	13	40	20	190		

**Table 4** — Inductor thermal model parameters

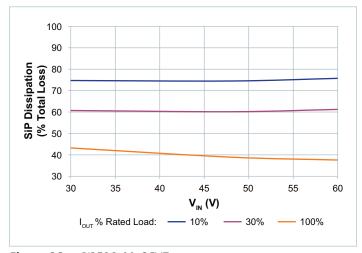
# **SiP Power Dissipation as Percentage of Total System Losses**



**Figure 84** — PI3583-00-QFYZ



**Figure 85** — PI3585-00-QFYZ



**Figure 86** — PI3586-00-QFYZ



## **Application Description**

#### **Output Voltage Set Point**

The PI358x-00 family of Buck Regulators utilizes  $V_{REF}$ , an internal reference for regulating the output voltage. The output voltage setting is accomplished using external resistors as shown in Figure 87. Select R2 to be at or around  $1k\Omega$  for best noise immunity. Use Equations 2 and 3 to determine the proper value based on the desired output voltage.

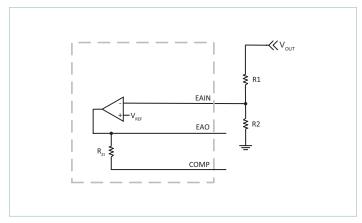


Figure 87 — External resistor divider network

$$V_{OUT} = V_{REF} \bullet \frac{R1 + R2}{R2} \tag{2}$$

$$R1 = R2 \bullet \frac{V_{OUT} - V_{REF}}{V_{REF}} \tag{3}$$

Where:

 $V_{RFF} = V_{FAIN}$ 

### **Soft Start Adjust and Tracking**

The TRK pin offers a means to adjust the regulator's soft-start time or to track with additional regulators. The soft-start slope is controlled by an external capacitor and a fixed charge current to provide a Soft-Start Time  $t_{SS}$  for all PI358x-00 regulators. The following equation can be used to calculate the proper capacitor for a desired soft-start times:

$$C_{TRK} = \left(t_{TRK} \bullet I_{TRK}\right) \tag{4}$$

where  $t_{TRK}$  is the soft-start time and  $I_{TRK}$  is a 50 $\mu$ A internal charge current (see Electrical Characteristics for limits).

There is typically either proportional or direct tracking implemented within a design. For proportional tracking between several regulators at start up, simply connect all PI358x-00 device TRK pins together. This type of tracking will force all connected regulators to start up and reach regulation at the same time (see Figure 88(a)).

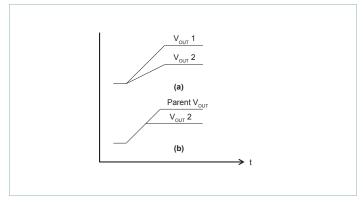


Figure 88 — PI358x-00 tracking responses

For Direct Tracking, choose the PI358x-00 with the highest output voltage as the parent and connect the parent to the TRK pin of the other PI358x-00 regulators through a divider (Figure 88) with the same ratio as the child's feedback divider.

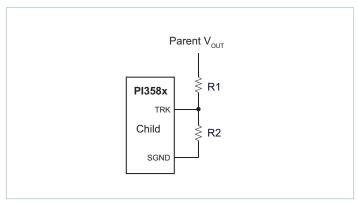


Figure 89 — Voltage divider connections for direct tracking

All connected PI358x-00 regulator soft-start slopes will track with this method. Direct tracking timing is demonstrated in Figure 88(b). All tracking regulators should have their Enable (EN) pins connected together to work properly.

## **Inductor Pairing**

The PI358x-00 utilizes an external inductor. This inductor has been optimized for maximum efficiency performance. Table 5 details the specific inductor value and part number utilized for each PI358x-00.

Product	Value	Mfr.	Part Number	Max Operating Temperature
System	(nH)	IVIII.	raitivuilibei	T <sub>INT-IND</sub> (°C)
PI3583-00-QFYZ	420	Eaton	HCV1206-R42-R	125
PI3585-00-QFYZ	420	Eaton	HCV1206-R42-R	125
PI3586-00-QFYZ	900	Eaton	HCV1206-R90-R	125

**Table 5** — PI358x-00 inductor pairing

#### **Parallel Operation**

Multiple PI358x-00 can be connected in parallel to increase the output capability of a single output rail. When connecting modules in parallel, each EAO, TRK and EN pin should be connected together. EAIN pins should remain separated, each with a REA1 and REA2, to reject noise differences between different modules' SGND pins. Current sharing will occur automatically in this manner so long as each inductor is the same value. Refer to the Electrical Characteristics table for maximum array size and array rated output current. Current sharing may be considered independent of synchronization and/or interleaving. Modules do not have to be interleaved or synchronized to share current.

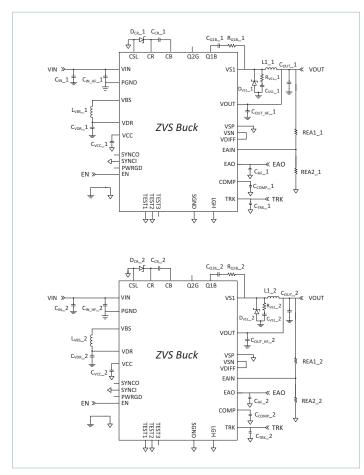


Figure 90 — PI358x-00 parallel operation

Due to the high output current capability of a single module and CrCM occurring at approximately 50% rated load, interleaving is not supported.

Use of the PI358x-00 SYNCI pin is practical only under a limited set of conditions. Synchronizing to another converter or to a fixed external clock source can result in a significant reduction in output power capability or higher than expected ripple.

#### **Filter Considerations**

The PI358x-00 requires low impedance ceramic input capacitors (X7R/X5R or equivalent) to ensure proper start up and high frequency decoupling for the power stage. The PI358x-00 will draw nearly all of the high frequency current from the low impedance ceramic capacitors when the main high side MOSFET(s) are conducting. During the time the MOSFET(s) are off, the input capacitors are replenished from the source.

Table 7 shows the recommended input and output capacitors to be used for the PI358x-00 as well as per capacitor RMS ripple current and the input and output ripple voltages. Table 6 lists the recommended input and output ceramic capacitors manufacturer and part numbers. It is very important to verify that the voltage supply source as well as the interconnecting lines are stable and do not oscillate.

# Input Filter Case 1 — Inductive source and local, external, input decoupling capacitance with negligible ESR (i.e.: ceramic type):

The voltage source impedance can be modeled as a series  $R_{\text{LINE}}$  circuit. The high performance ceramic decoupling capacitors will not significantly damp the network because of their low ESR; therefore in order to guarantee stability the following conditions must be verified:

$$R_{LINE} > \frac{L_{LINE}}{C_{IN} \cdot \left| r_{EQ\_IN} \right|} \tag{5}$$

$$R_{LINE} \ll \left| r_{EO\ IN} \right| \tag{6}$$

Where  $r_{EQ\_IN}$  can be calculated by dividing the lowest line voltage by the full load input current. It is critical that the line source impedance be at least an octave lower than the converter's dynamic input resistance, Equation 6. However,  $R_{LINE}$  cannot be made arbitrarily low otherwise Equation 5 is violated and the system will show instability, due to an under-damped RLC input network.

# Input Filter case 2 — Inductive source and local, external input decoupling capacitance with significant $R_{C_{IN}}$ ESR (i.e., electrolytic type):

In order to simplify the analysis in this case, the voltage source impedance can be modeled as a simple inductor  $L_{\text{LINF}}$ .

Notice that the high performance ceramic capacitors  $C_{IN\_INT}$  within the PI358x-00 should be included in the external electrolytic capacitance value for this purpose. The stability criteria will be:

$$\left| r_{EO\ IN} \right| > R_{C_{IN}} \tag{7}$$

$$\frac{L_{LINE}}{C_{IN} \cdot R_{C_{IN}}} < \left| r_{EQ\_IN} \right| \tag{8}$$

Equation 8 shows that if the aggregate ESR is too small – for example by using very high quality input capacitors ( $C_{\rm IN}$ ) – the system will be under-damped and may even become destabilized. As noted, an octave of design margin in satisfying Equation 7 should be considered the minimum. When applying an electrolytic capacitor for input filter damping the ESR value must be chosen to avoid loss of converter efficiency and excessive power dissipation in the electrolytic capacitor.



#### **VDR Bias Regulator**

The VDR bias regulator is a ZVS switching regulator that is intended primarily to power the internal controller and driver circuitry. The power capability of this regulator is sized for the PI358x-00, with adequate reserve for the application it was intended for.

It may be used for as a pullup source for open collector applications and for other very low power uses with the following restrictions:

- **1.** The total external loading on VDR must be less than  $I_{VDR}$ .
- 2. No direct connection is allowed. Any noise source that can disturb the VDR voltage can also affect the internal controller operation. A series impedance is required between the VDR pin and any external circuitry.
- **3.** All loads must be locally decoupled using a  $0.1\mu F$  ceramic capacitor. This capacitor must be connected to the VDR output through a series resistor no smaller than  $1k\Omega$ , which forms a low-pass filter.

#### **Additional System Design Considerations**

- **1.** Inductive loads: As with all power electronic applications, consideration must be given to driving inductive loads that may be exposed to a fault in the system which could result in consequences beyond the scope of the power supply primary protection mechanisms. An inductive load could be a filter, fan motor or even excessively long cables. Consider an instantaneous short circuit through an un-damped inductance that occurs when the output capacitors are already at an initial condition of fully charged. The only thing that limits the current is the inductance of the short circuit and any series resistance. Even if the power supply is off at the time of the short circuit, the current could ramp up in the external inductor and store considerable energy. The release of this energy will result in considerable ringing, with the possibility of ringing nodes connected to the output voltage below ground. The system designer should plan for this by considering the use of other external circuit protection such as load switches, fuses, and transient voltage protectors. The inductive filters should be critically damped to avoid excessive ringing or damaging voltages. Adding a high current Schottky diode from the output voltage to PGND close to the PI358x-00 is recommended for these applications.
- 2. Low voltage operation: There is no isolation from an SELV (Safety-Extra-Low-Voltage) power system. Powering low voltage loads from input voltages as high as 60V may require additional consideration to protect low voltage circuits from excessive voltage in the event of a short circuit from input to output. A fast TVS (transient voltage suppressor) gating an external load switch is an example of such protection.

Input / Output	Manufacturer	Manufacturer Part Number		Description
	Murata	GRM32EC70J107ME15	100μF	100µF 6.3V 1210 X7S
Output	Murata	GRM32ER71A476KE15	47μF	47μF 10V 1210 X7R
	Murata	GRM32DR71E106KA12	10μF	10μF 25V 1210 X7R
land.	Murata	GRM32ER72A225KA35	2.2µF	2.2µF 100V 1210 X7R
Input	<b>or</b> Murata	GRM32ER71K475KE14L	4.7µF	4.7µF 80V 1210 X7R

**Table 6** — Recommended input and output capacitor components

Product	Load Current (A)	C <sub>IN</sub>	С <sub>оит</sub>	C <sub>IN</sub> Ripple Current (A <sub>RMS</sub> )	C <sub>OUT</sub> Ripple Current (A <sub>RMS</sub> )	V <sub>IN</sub> Ripple (mV <sub>P-P</sub> )	V <sub>OUT</sub> Ripple (mV <sub>P-P</sub> )	Load Step (A) (1A/µs)	V <sub>OUT</sub> Droop and Kick (mV <sub>PP</sub> )	V <sub>OUT</sub> Recovery Time (µs)
PI3583	10	6 x 2.2μF	6 x 100μF	3.3	7.0	430	40	5	160	80
PI3585	10	6 x 2.2μF	6 x 47μF	4.3	8.3	380	60	5	130	80
PI3586	10	6 x 2.2μF	6 x 10µF	5	6.0	600	140	4.5	330	80

**Table 7** — Recommended input and output capacitor quantity and performance



## **Layout Guidelines**

To optimize maximum efficiency and low noise performance from a PI358x-00 design, layout considerations are necessary. Reducing trace resistance and minimizing high current loop returns along with proper component placement will contribute to optimized performance.

A typical buck converter circuit is shown in Figure 91. The potential areas of high parasitic inductance and resistance are the circuit return paths, shown as LR below.

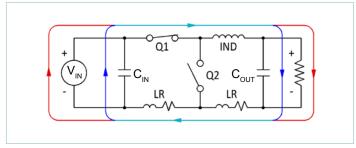


Figure 91 — Typical buck regulator

The path between the  $C_{OUT}$  and  $C_{IN}$  capacitors is of particular importance since the AC currents are flowing through both of them when Q1 is turned on. Figure 92, schematically, shows the reduced trace length between input and output capacitors. The shorter path lessens the effects that copper trace parasitics can have on the PI358x-00 performance.

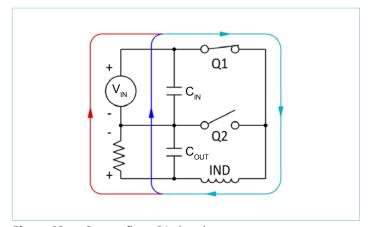


Figure 92 — Current flow: Q1 closed

When Q1 is on and Q2 is off, the majority of  $C_{IN}$ 's current is used to satisfy the output load and to recharge the  $C_{OUT}$  capacitors. When Q1 is off and Q2 is on, the load current is supplied by the inductor and the  $C_{OUT}$  capacitor as shown in Figure 93. During this period  $C_{IN}$  is also being recharged by the  $V_{IN}$ . Minimizing  $C_{IN}$  loop inductance is important to reduce peak voltage excursions when Q1 turns off. Also, the difference in area between the  $C_{IN}$  loop and  $C_{OUT}$  loop is vital to minimize switching and GND noise.

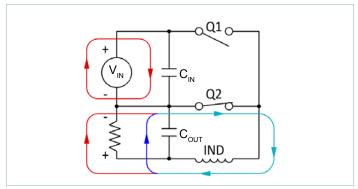
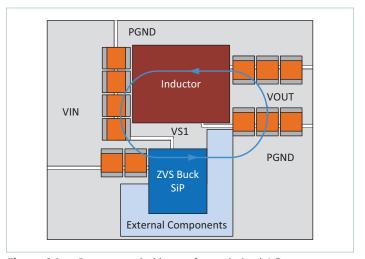


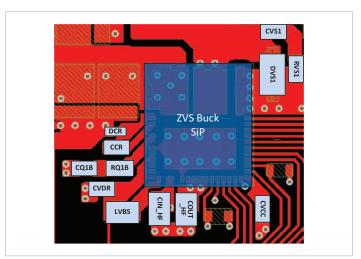
Figure 93 — Current flow: Q2 closed

Figure 94 illustrates the tight path between  $C_{\rm IN}$  and  $C_{\rm OUT}$  (and  $V_{\rm IN}$  and  $V_{\rm OUT}$ ) for the high AC return current. The external  $C_{\rm IN}$  capacitor needs to be connected to the input of the SiP through a low inductance connection, which is especially important due to the lack of internal input capacitance. The PI358x-00 evaluation board uses a layout optimized for performance in this way.



**Figure 94** — Recommended layout for optimized AC current within the SiP, inductor, and ceramic input and output capacitors

Besides the critical power path involving the input/output of the converter, the input/output capacitors and the inductor, the routing of some powertrain supporting components are also sensitive to routing parasitics. For example,  $L_{VBS}$  and  $C_{VDR}$  are passive components for internal bias supply switcher;  $D_{VS1}$ ,  $C_{VS1}$  and  $R_{VS1}$  are clamped to protect VS1, the main switching node. In either condition, a path with low inductance is required.



**Figure 95** — Example layout of external components on a Pl358x evaluation board

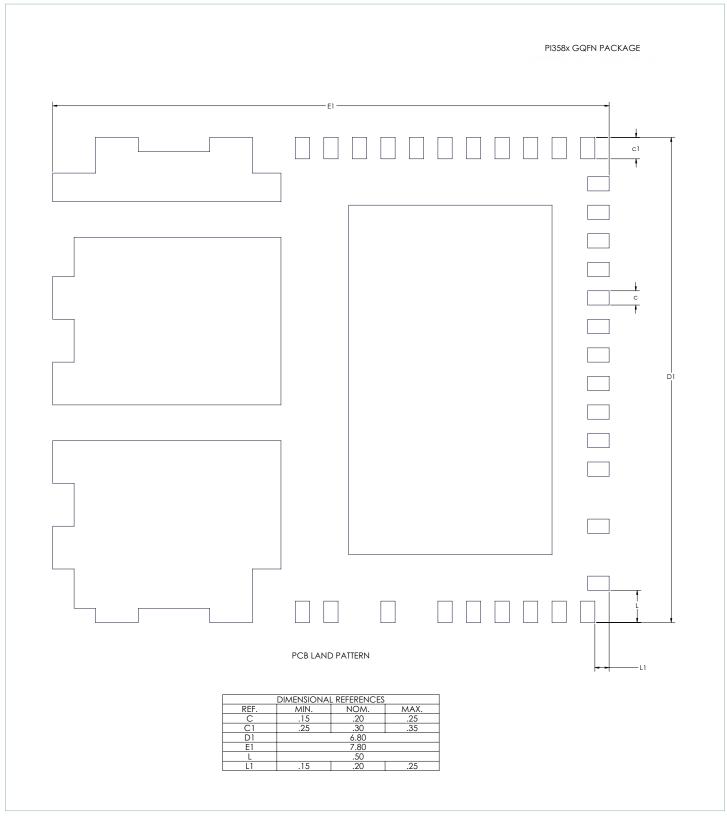
Here is a list of external components to the SiP which needs to have low inductance routes:

 $C_{OUT\_HF}$ ,  $C_{IN\_HF}$ ,  $C_{Q1B}$ ,  $R_{Q1B}$ ,  $D_{CR}$ ,  $C_{CR}$ ,  $D_{VS1}$ ,  $C_{VS1}$ ,  $R_{VS1}$ ,  $L_{VBS}$ ,  $C_{VDR}$ ,  $C_{VCC}$ . An example layout from the evaluation board is shown in Figure 95. These external components are placed locally to the SiP and connect to the relevant pin with wide traces. Some of them have the other end connecting through vias to the ground plane in the underneath layer. A similar practice is expected in customer applications.

In many cases the powertrain or its related layout is critical and sensitive to routing parasitics. A direct copy of the Vicor reference PCB layout is recommended.



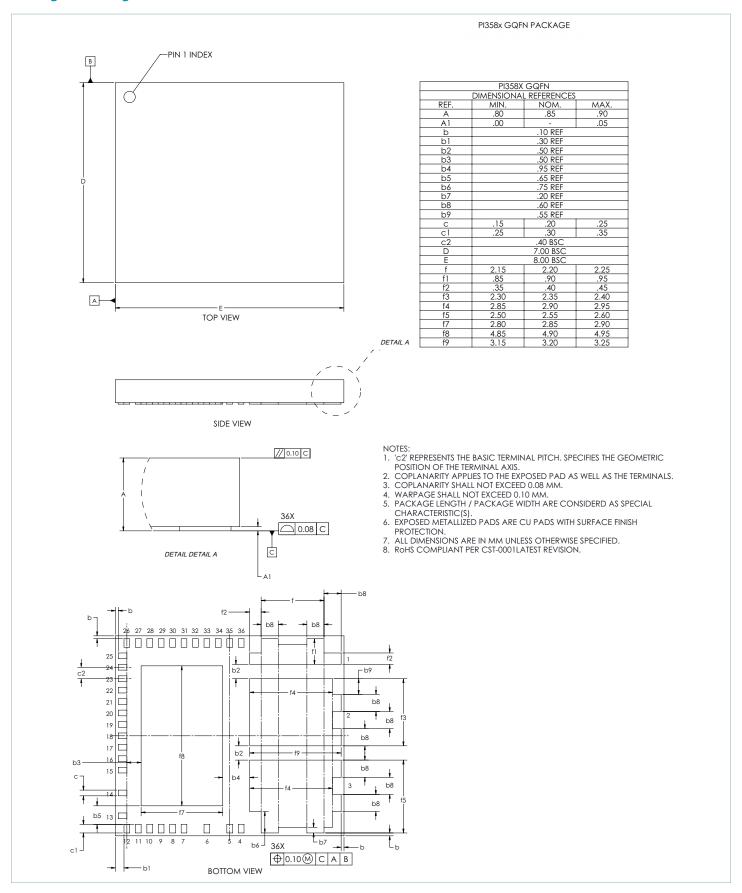
# **Recommended PCB Footprint**



Recommended receiving footprint for PI358x-00 7 x 8mm package.



## **Package Drawings**



# **Revision History**

Revision	Date	Description	Page Number(s)
1.0	02/25/19	Initial release	n/a
1.1	06/23/20	Updated outline drawing	43
1.2	08/11/20	Updated terminology	37



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