## QPO-1-EVAL1

QPO ${ }^{\text {™ }}$ Active Output Filter Evaluation Board


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Figure 1
Top view of evaluation board

## Introduction

The QPO-1-EVAL1 is designed to allow full testing of the QPO-1LZ, along with its various performance options, to fully optimize a final system design. The board offers two terminal options for vertical or horizontal mounting. The user must select the required values for the RHR, RSCSET and RSA resistors and solder them in the designated positions before applying power to the EVAL1. Please refer to the QPO-1LZ product data sheet, schematics and the following pages for the proper application of this board.

The QPO-1 output ripple attenuator SiP uses active filtering to reduce output ripple and noise (PARD) over 30 dB from 500 Hz to 500 kHz and can be extended down to 50 Hz with additional capacitance added to the VREF pin. The QPO-1LZ operates over a voltage range from 3 to $30 \mathrm{~V}_{\mathrm{DC}}$ and supports load currents as high as 10A. Output regulation is maintained with remote sense or trim adjustment of the power supply. The closed loop architecture improves transient response and ensures quiet point-of-load regulation when used in conjunction with the power supply's control loop or trim node.

## Features

- > 30dB PARD attenuation, 1 - 500kHz
- $3-30 V_{D C}$ operating range
- 10A rating
- Supports precise point-of-load regulation through use of remote sensing or converter trimming
- Optional start-up circuit included
- User-selectable performance optimization for attenuation, power dissipation and transient response
- Horizontal or vertical mounting options
- Evaluation board includes a Johnson Jack for low-noise measurement of the QPO's filtering performance



## QPO-1 Performance

The waveforms in Figure 2 highlight the QPO-1's ability to both filter a converter's output ripple and maintain a constant output voltage during a load transient. The input voltage of the QPO-1 (dark blue) shows varying amplitude and frequency PARD before and during the load transient, but the QPO-1 output voltage (light blue) remains relatively unaffected. The load transient is a 1 -10A load step (green).

The converter used is a Vicor Mini, 48V to 5V converter (Model number: V48B5C200BN).
Figure 2

Figure 3
Evaluation board schematic


## QPO-1-EVAL1 BOM

| Qty | Description | Value | Designator | Vendor | Vendor Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | Capacitor, X7R eramic, $15 \mu \mathrm{~F}, 25 \mathrm{~V}$, 1812 | $15 \mu \mathrm{~F}$ | C1, CESR | TDK | C4532X7R1E156MT |
| 1 | Capacitor, X7R Ceramic, 1 $\mu \mathrm{F}, 50 \mathrm{~V}, 1206$ | $1 \mu \mathrm{~F}$ | CSU | TDK | C3216X7R1H105K |
| 1 | Diode, Zener, 12V, 0.15W, SOT-23 | 18V | DZ1 | ON Semi | BZX84C18LT1G |
| 8 | Samtec, 0.2 in , Rt-Angle Header |  | $\begin{aligned} & \mathrm{J} 1, \mathrm{~J}, \mathrm{~J} 3, \mathrm{~J} 4, \\ & \mathrm{~J} 5, \mathrm{~J} 6, \mathrm{~J} 7, \mathrm{~J} 8 \end{aligned}$ | Samtec | FWS-08-02-T-S-RA |
| 2 | Connector, Johnson Jack | Johnson Jack | J11, J12 | Tektronix | 131503100 |
| 1 | Transistor, PFET, 30V, 0.6A | RLML5103TRPBF | Q1 | International Recifier | IRLML5103TRPB ${ }^{\text {F }}$ |
| 1 | QPO-1LZ | QPO-1LZ | QPO-1 | VICOR | QPO-1LZ |
| 1 | Resistor, 5\%, 0.25W, 1206 | 100 | R2 | Rohm | MCR18EZPJ101 |
| 1 | Resistor, 5\%, 0.25W, 1206 | $1.00 \mathrm{k} \Omega$ | RP | Rohm | MCR18EZHF1001 |
| 1 | Resistor, 5\%, 0.25W, 1206 | 51.1 | RSENSE | Rohm | MCR18EZPF51R1 |
| 1 | Resistor, 1\%, 0.25W, 1206 | $20 \mathrm{k} \Omega$ | RSU | Rohm | MCR18EZHF2002 |

## Installed Components

The QPO-1-EVAL1 board comes with the following components pre-stuffed:

Remote Sense Components
C1, RSENSE
Start-up Assist Circuit
CSU, RSU, DZ1, R2, Q1
Peak Detector
CESR

RP
CESR

## User-Defined Components

The QPO-1-EVAL1 board comes with the following components not installed; values to be determined by customer:

| Headroom Resistor | RHR (not optional, must be installed for proper operation) |
| :--- | :--- |
| Headroom Capacitor | CHR (optional) |
| Slope Adjust | RSA (optional) |
| SC Function | CSC, RSCSET (optional) |
| Peak Detector | CP (optional) |

## Function Descriptions

## Slope Adjust

The slope adjust function allows the user to modify the voltage drop across the QPO-1 (headroom voltage) dependent on the current passing through the QPO-1. This function is used to maintain a constant power across the QPO-1 over a varying range of load currents. The RSA resistor can be calculated by using the following equation:

$$
\begin{equation*}
R_{S A}=\frac{0.05 \mathrm{~V}}{A} \cdot \frac{\Delta I_{O U T}}{\Delta V_{H R}} \cdot 2.5 \mathrm{k} \Omega \tag{1}
\end{equation*}
$$

Where:

$$
\begin{aligned}
& \Delta \mathrm{l}_{\text {OUT }}=\text { Maximum change in load current }(\mathrm{A}) \\
& \Delta \mathrm{V}_{\mathrm{HR}}=\text { headroom voltage change over load range }(\mathrm{V}) \\
& \mathrm{R}_{\mathrm{SA}}=\text { slope adjust resistor }(\Omega)
\end{aligned}
$$

The slope adjust feature can be disabled by either using a large resistor value ( $100 \mathrm{k} \Omega$ or greater) for $\mathrm{R}_{\text {SA }}$ or by omitting this resistor entirely.

## Headroom Adjust

The RHR resistor is used to program the desired voltage drop across the QPO-1. This voltage must be greater than the ripple voltage that the QPO-1 is to filter, with additional voltage added for the voltage drops in the attenuation path. Like the RP resistor, the RHR resistor must always be installed for proper operation. The value of $\mathrm{R}_{\mathrm{HR}}$ can be calculated using this equation:

$$
\begin{equation*}
R_{H R}=\frac{Q P O_{O U T} \cdot 2.5 \mathrm{k} \Omega}{V_{H R}} \tag{2}
\end{equation*}
$$

Where:

$$
\begin{aligned}
& \mathrm{R}_{\mathrm{HR}}=\text { headroom setting resistor value }(\Omega) \\
& \mathrm{QPO}_{\mathrm{OUT}}=\text { the voltage on the QPO's output }(\mathrm{V}) \\
& \mathrm{V}_{\mathrm{HR}}=\text { the target headroom voltage }(\mathrm{V})
\end{aligned}
$$

If this resistor is omitted, then the reference pin will be at the same voltage as the input pin, forcing the output pin to be the same voltage as the input pin.

## SC Function

The function of the SC circuit is to use a converter's trim or SC (secondary control) pin to compensate for the voltage drop across the QPO-1, thereby maintaining the desired output voltage on the QPO's output.
The RSCSET resistor (listed as RSC in the data sheet) determines the amount of current the SC pin of the QPO-1 will source. The current is calculated by dividing the headroom voltage (the voltage drop from $\mathrm{QPO}_{\text {IN }}$ to $\mathrm{QPO}_{\text {OUt }}$ ) by $\mathrm{R}_{\text {SCSET }}$.

$$
\begin{equation*}
R_{S C S E T}=\frac{R_{I N} \bullet V_{O U T}}{V_{R P T}} \tag{3}
\end{equation*}
$$

Where:

$$
\begin{aligned}
& \mathrm{V}_{\text {OUT }}=\text { nominal converter output voltage }(\mathrm{V}) \\
& \mathrm{V}_{\text {RPT }}=\text { internal reference voltage }(\mathrm{V}) \\
& \mathrm{R}_{\mathrm{IN}}=\text { internal series resistor }(\Omega)
\end{aligned}
$$

When using one of the Vicor Micro, Mini or Maxi converters, the $R_{I N}=1 \mathrm{k} \Omega$ and the $\mathrm{V}_{\text {RPT }}=1.23 \mathrm{~V}$.
Figure 4 shows the QPO-1-EVAL1 board connected so as to use the SC function to compensate for the QPO-1's voltage drop.

## Remote Sense

Compensation for the QPO-1's voltage drop can be done using the converter's remote-sense pins, if available. The on-board sensing network can be attached as is shown in Figure 5.

Figure 4
Evaluation board in SC configuration


Figure 5
Evaluation board in remote-sense configuration


Figure 6
Start-up waveforms; without (top) and with (bottom) the optional start-up circuit

## Start-up Circuit

The start-up circuit (Figure 3) on the evaluation board is used to connect the QPO-1's reference pin to its input pin during start up. In both waveform pictures of Figure 6, the Output Voltage (light blue) follows the $\mathrm{V}_{\text {REF }}$ voltage (purple) of the QPO-1.

In the picture on the top in Figure 6, without the optional start-up circuit, the QPO-1 input voltage (the converter's output voltage) can be seen to be greater than the nominal 5 V output of the converter. This is due to the QPO-1's SC circuit having greater headroom voltage during start up and therefore over-driving the SC of the converter. After about 40 ms , the $\mathrm{V}_{\text {REF }}$ voltage reaches its 5 V pre-set limit and the converter's output voltage starts to drop, eventually steadying out at 5.35 V , the nominal output voltage plus the QPO-1's headroom voltage.

The potential problem with this start up is that the converter could fault due to its output being forced to be greater than $110 \%$ of the nominal value. For converters with lower nominal output voltages, this could be very serious condition.

The waveforms on the bottom are the same converter with the optional start-up circuit enabled. Here, the $\mathrm{V}_{\text {REF }}$ is forced to follow $\mathrm{V}_{\text {IN }}$, so $\mathrm{V}_{\text {Out }}$ follows as well. After about 25 ms , the start-up circuit releases the VREF pin and it adjusts it value down to generate the proper headroom voltage across the QPO-1. Using this method, there is no possibility of over-driving the converter and causing a fault.

## Peak Detector

The QPO-1 peak detector is used to adapt the headroom voltage in response to increasing converter ripple. The greater the ripple on the QPO-1's input, the greater the headroom voltage across the QPO-1. This feature can be disabled by adding the CP capacitor to the evaluation board. The addition of this capacitor creates an RC filter network that filters out the converter's ripple to the peak detector.

The RP resistor must always be installed for proper operation. The peak detector creates the internal reference voltage rail that gets divided down by the headroom resistor RHR.

Figure 7
Mounting options


Figure 8
Mechanical drawing


Ordering Information

## Carrier Board Part Number Compatible VI Chip ${ }^{\circledR}$ Evaluation Boards (sold separately) ${ }^{[b]}$

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