

**GENERAL DESCRIPTION**

This amplifier has ultralow offset, drift, and bias current.

The AD8628/AD8629/AD8630 are wide bandwidth auto-zero amplifiers featuring rail-to-rail input and output swing and low noise. Operation is fully specified from 2.7 V to 5 V single supply ( $\pm 1.35$  V to  $\pm 2.5$  V dual supply).

The AD8628/AD8629/AD8630 provide benefits previously found only in expensive auto-zeroing or chopper-stabilized amplifiers.

With an offset voltage of only 1  $\mu$ V, drift of less than 0.005  $\mu$ V/ $^{\circ}$ C, and noise of only 0.5  $\mu$ V p-p (0 Hz to 10 Hz), the AD8628/AD8629/AD8630 are suited for applications where error sources cannot be tolerated. Position and pressure sensors, medical equipment, and strain gage amplifiers benefit greatly from nearly zero drift over their operating temperature range. Many systems can take advantage of the rail-to-rail input and output swings provided by the AD8628/AD8629/AD8630 to reduce input biasing complexity and maximize SNR.

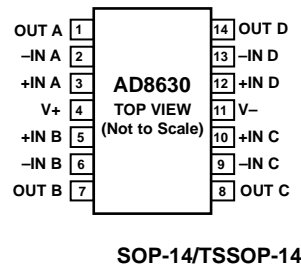
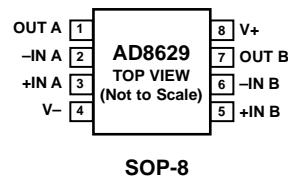
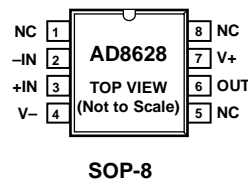
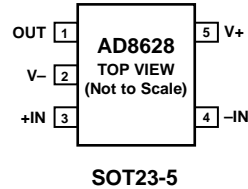
**FEATURES**

- Lowest auto-zero amplifier noise
- Low offset voltage: 1  $\mu$ V
- Input offset drift: 0.002  $\mu$ V/ $^{\circ}$ C
- Rail-to-rail input and output swing
- 5 V single-supply operation
- High gain, CMRR, and PSRR: 130 dB
- Very low input bias current: 100 pA
- maximum Low supply current: 1.0 mA
- Overload recovery time: 50  $\mu$ s
- No external components required

**APPLICATIONS**

- Automotive sensors
- Pressure and position sensors
- Strain gage amplifiers
- Medical instrumentation
- Thermocouple amplifiers
- Precision current sensing
- Photodiode amplifiers

**PIN CONFIGURATIONS**



## Zero-Drift, Single-Supply, Rail-to-Rail Input/Output Operational Amplifier

### SPECIFICATIONS ELECTRICAL CHARACTERISTICS— $V_S = 5.0\text{ V}$

$V_S = 5.0\text{ V}$ ,  $V_{CM} = 2.5\text{ V}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise noted.

Parameter	Symbol	Conditions	Min	Typ	Max	Unit
<b>INPUT CHARACTERISTICS</b>						
Offset Voltage	$V_{OS}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		1	5 10	$\mu\text{V}$ $\mu\text{V}$
Input Bias Current AD8628/AD8629 AD8630	$I_B$			30 100	100 300	$\mu\text{A}$ $\mu\text{A}$
Input Offset Current	$I_{OS}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		50	1.5 200	$\text{nA}$ $\mu\text{A}$
Input Voltage Range		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	0		250 5	$\mu\text{A}$ $\text{V}$
Common-Mode Rejection Ratio	CMRR	$V_{CM} = 0\text{ V to } 5\text{ V}$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	120 115	140 130		$\text{dB}$ $\text{dB}$
Large Signal Voltage Gain	$A_{VO}$	$R_L = 10\text{ k}\Omega$ , $V_O = 0.3\text{ V to } 4.7\text{ V}$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	125 120	145 135		$\text{dB}$ $\text{dB}$
Offset Voltage Drift	$\Delta V_{OS}/\Delta T$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		0.002	0.02	$\mu\text{V}/^\circ\text{C}$
<b>OUTPUT CHARACTERISTICS</b>						
Output Voltage High	$V_{OH}$	$R_L = 100\text{ k}\Omega$ to ground $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	4.99 4.99	4.996 4.995		$\text{V}$ $\text{V}$
		$R_L = 10\text{ k}\Omega$ to ground $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	4.95 4.95	4.98 4.97		$\text{V}$ $\text{V}$
Output Voltage Low	$V_{OL}$	$R_L = 100\text{ k}\Omega$ to $V_+$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		1 2	5 5	$\text{mV}$ $\text{mV}$
		$R_L = 10\text{ k}\Omega$ to $V_+$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		10 15	20 20	$\text{mV}$ $\text{mV}$
Short-Circuit Limit	$I_{SC}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	$\pm 25$	$\pm 50$ $\pm 40$		$\text{mA}$ $\text{mA}$
Output Current	$I_O$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		$\pm 30$ $\pm 15$		$\text{mA}$ $\text{mA}$
<b>POWER SUPPLY</b>						
Power Supply Rejection Ratio	PSRR	$V_S = 2.7\text{ V to } 5.5\text{ V}$ , $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	115	130		$\text{dB}$
Supply Current per Amplifier	$I_{SY}$	$V_O = V_S/2$ $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		0.85 1.0	1.1 1.2	$\text{mA}$ $\text{mA}$
<b>INPUT CAPACITANCE</b>						
Differential	$C_{IN}$			1.5		$\text{pF}$
Common Mode				8.0		$\text{pF}$
<b>DYNAMIC PERFORMANCE</b>						
Slew Rate	SR	$R_L = 10\text{ k}\Omega$		1.0		$\text{V}/\mu\text{s}$
Overload Recovery Time				0.05		$\text{ms}$
Gain Bandwidth Product	GBP			2.5		$\text{MHz}$
<b>NOISE PERFORMANCE</b>						
Voltage Noise	$e_n$ p-p	0.1 Hz to 10 Hz		0.5		$\mu\text{V p-p}$
		0.1 Hz to 1.0 Hz		0.16		$\mu\text{V p-p}$
Voltage Noise Density	$e_n$	$f = 1\text{ kHz}$		22		$\text{nV}/\sqrt{\text{Hz}}$
Current Noise Density	$i_n$	$f = 10\text{ Hz}$		5		$\text{fA}/\sqrt{\text{Hz}}$

## Zero-Drift, Single-Supply, Rail-to-Rail Input/Output Operational Amplifier

### ELECTRICAL CHARACTERISTICS— $V_S = 2.7\text{ V}$

$V_S = 2.7\text{ V}$ ,  $V_{CM} = 1.35\text{ V}$ ,  $V_O = 1.4\text{ V}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise noted.

Parameter	Symbol	Conditions	Min	Typ	Max	Unit
<b>INPUT CHARACTERISTICS</b>						
Offset Voltage	$V_{OS}$			1	5	$\mu\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			10	$\mu\text{V}$
Input Bias Current	$I_B$					
AD8628/AD8629				30	100	$\text{pA}$
AD8630				100	300	$\text{pA}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		1.0	1.5	$\text{nA}$
Input Offset Current	$I_{OS}$			50	200	$\text{pA}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			250	$\text{pA}$
Input Voltage Range			0		2.7	$\text{V}$
Common-Mode Rejection Ratio	CMRR	$V_{CM} = 0\text{ V to } 2.7\text{ V}$	115	130		$\text{dB}$
Large Signal Voltage Gain	$A_{VO}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	110	120		$\text{dB}$
		$R_L = 10\text{ k}\Omega$ , $V_O = 0.3\text{ V to } 2.4\text{ V}$	110	140		$\text{dB}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	105	130		$\text{dB}$
Offset Voltage Drift	$\Delta V_{OS}/\Delta T$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		0.002	0.02	$\mu\text{V}/^\circ\text{C}$
<b>OUTPUT CHARACTERISTICS</b>						
Output Voltage High	$V_{OH}$	$R_L = 100\text{ k}\Omega$ to ground	2.68	2.695		$\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	2.68	2.695		$\text{V}$
		$R_L = 10\text{ k}\Omega$ to ground	2.67	2.68		$\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	2.67	2.675		$\text{V}$
Output Voltage Low	$V_{OL}$	$R_L = 100\text{ k}\Omega$ to $V_+$		1	5	$\text{mV}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		2	5	$\text{mV}$
		$R_L = 10\text{ k}\Omega$ to $V_+$		10	20	$\text{mV}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		15	20	$\text{mV}$
Short-Circuit Limit	$I_{SC}$		$\pm 10$	$\pm 15$		$\text{mA}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		$\pm 10$		$\text{mA}$
Output Current	$I_O$			$\pm 10$		$\text{mA}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			$\pm 5$	$\text{mA}$
<b>POWER SUPPLY</b>						
Power Supply Rejection Ratio	PSRR	$V_S = 2.7\text{ V to } 5.5\text{ V}$ , $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	115	130		$\text{dB}$
Supply Current per Amplifier	$I_{SY}$	$V_O = V_S/2$		0.75	1.0	$\text{mA}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		0.9	1.2	$\text{mA}$
<b>INPUT CAPACITANCE</b>						
Differential				1.5		$\text{pF}$
Common Mode				8.0		$\text{pF}$
<b>DYNAMIC PERFORMANCE</b>						
Slew Rate	SR	$R_L = 10\text{ k}\Omega$		1		$\text{V}/\mu\text{s}$
Overload Recovery Time				0.05		$\text{ms}$
Gain Bandwidth Product	GBP			2		$\text{MHz}$
<b>NOISE PERFORMANCE</b>						
Voltage Noise	$e_n$ p-p	0.1 Hz to 10 Hz		0.5		$\mu\text{V p-p}$
Voltage Noise Density	$e_n$	$f = 1\text{ kHz}$		22		$\text{nV}/\sqrt{\text{Hz}}$
Current Noise Density	$i_n$	$f = 10\text{ Hz}$		5		$\text{fA}/\sqrt{\text{Hz}}$

TYPICAL PERFORMANCE CHARACTERISTICS

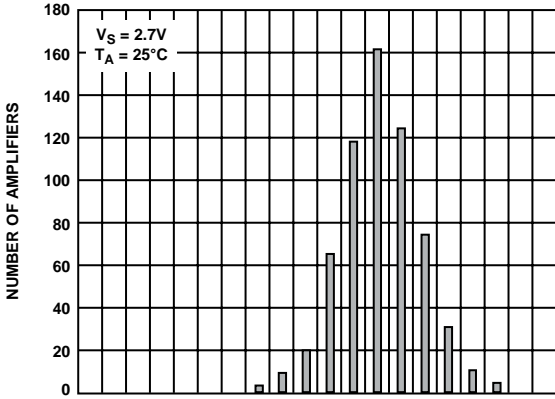


Figure 5. Input Offset Voltage Distribution

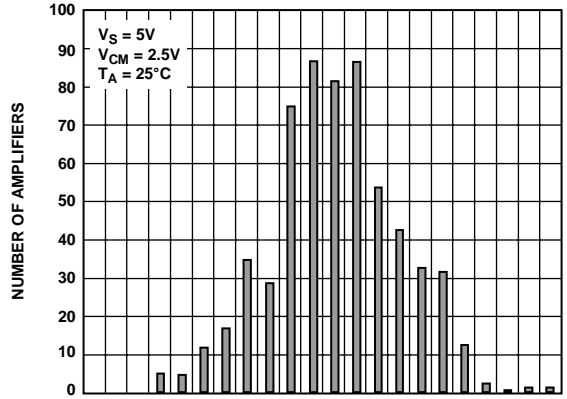


Figure 8. Input Offset Voltage Distribution

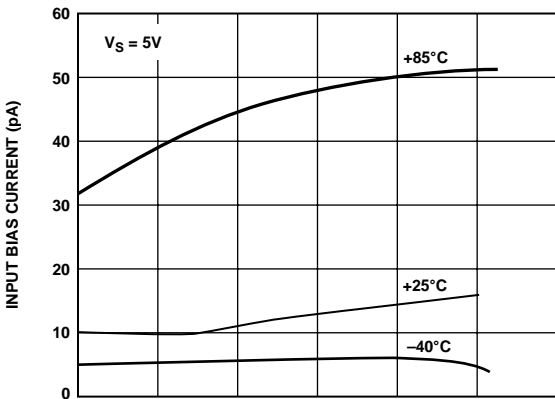


Figure 6. AD8628 Input Bias Current vs. Input Common-Mode Voltage

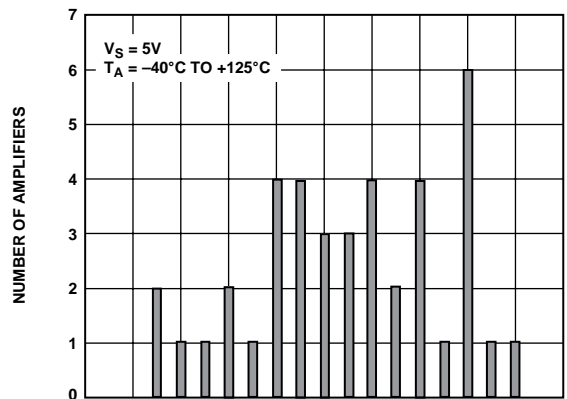


Figure 9. Input Offset Voltage Drift

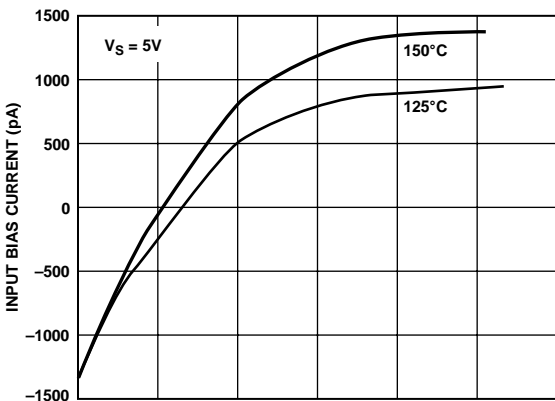


Figure 7. AD8628 Input Bias Current vs. Input Common-Mode Voltage

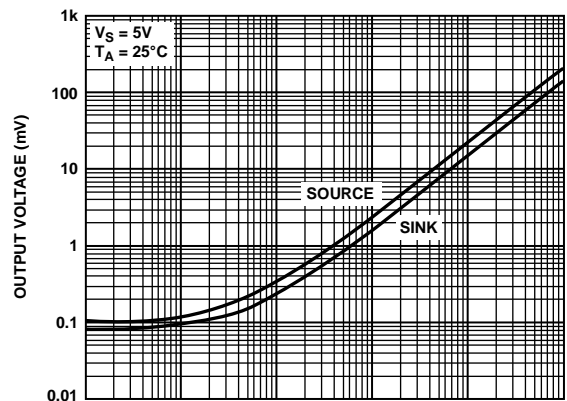


Figure 10. Output Voltage to Supply Rail vs. Load Current

Zero-Drift, Single-Supply, Rail-to-Rail Input/Output Operational Amplifier

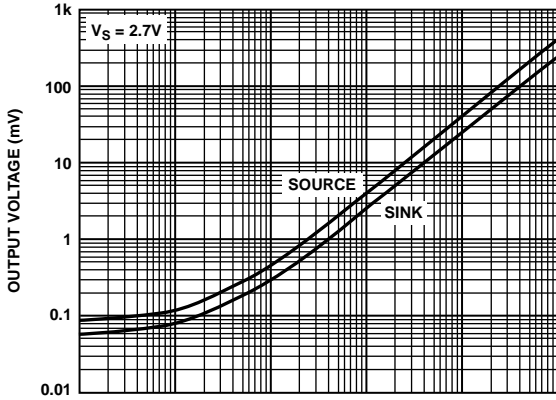


Figure 11. Output Voltage to Supply Rail vs. Load Current

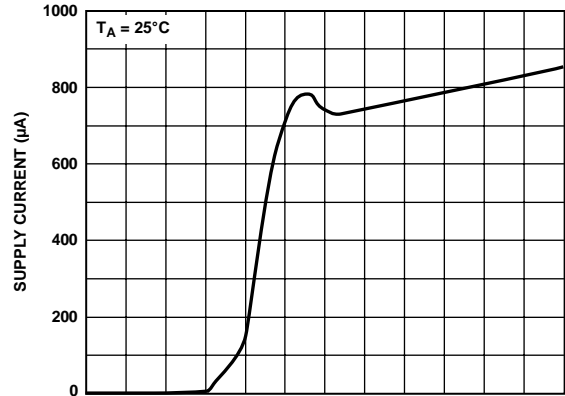


Figure 14. Supply Current vs. Supply Voltage

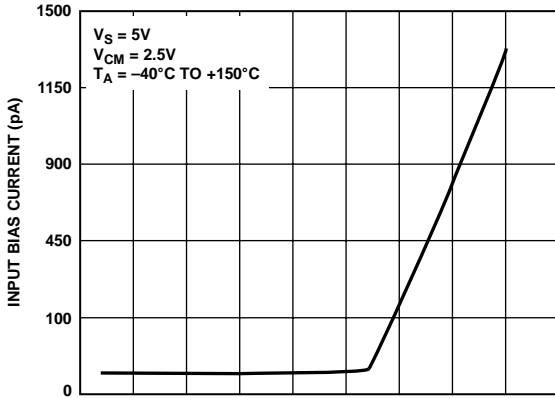


Figure 12. AD8628 Input Bias Current vs. Temperature

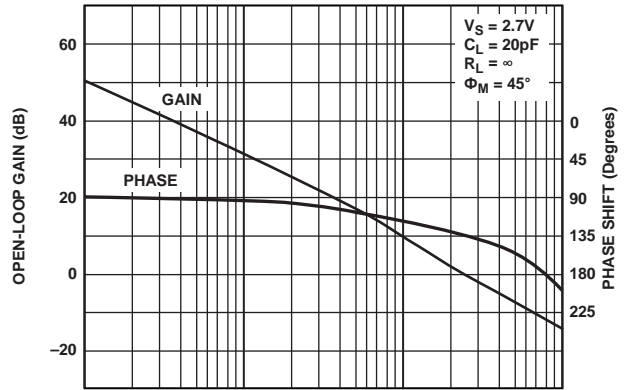


Figure 15. Open-Loop Gain and Phase vs. Frequency

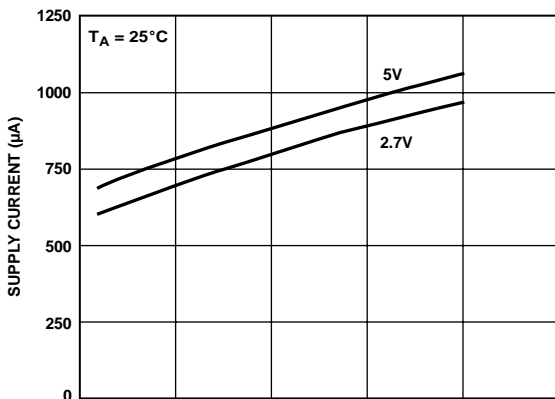


Figure 13. Supply Current vs. Temperature

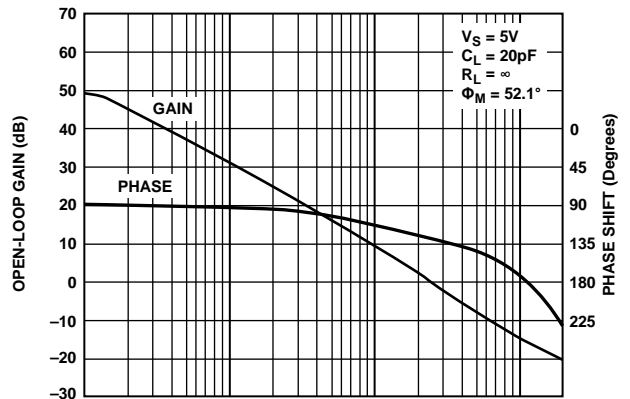


Figure 16. Open-Loop Gain and Phase vs. Frequency

Zero-Drift, Single-Supply, Rail-to-Rail Input/Output Operational Amplifier

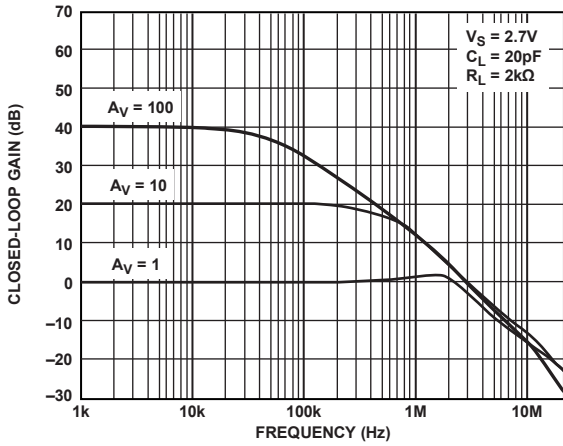


Figure 17. Closed-Loop Gain vs. Frequency

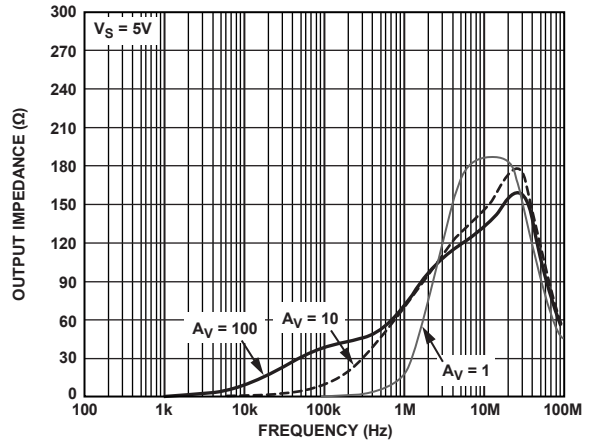


Figure 20. Output Impedance vs. Frequency

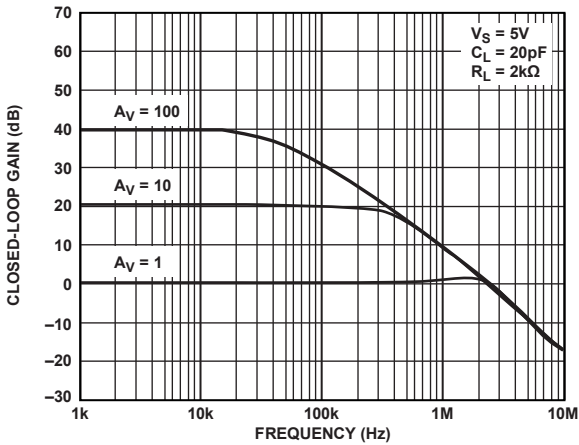


Figure 18. Closed-Loop Gain vs. Frequency

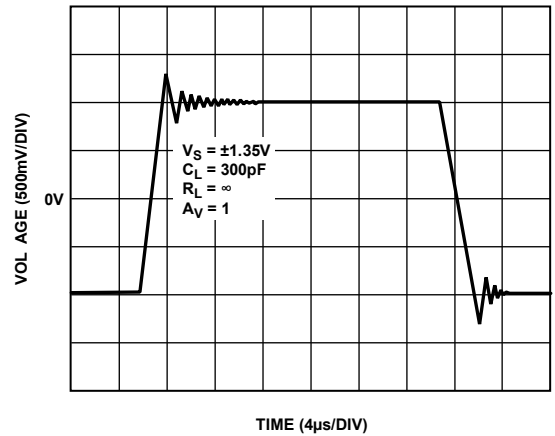


Figure 21. Large Signal Transient Response

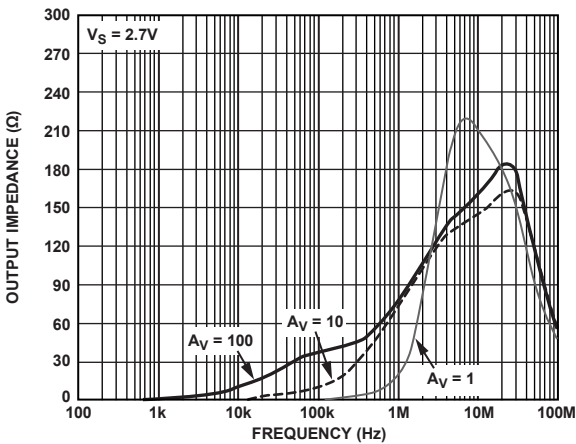


Figure 19. Output Impedance vs. Frequency

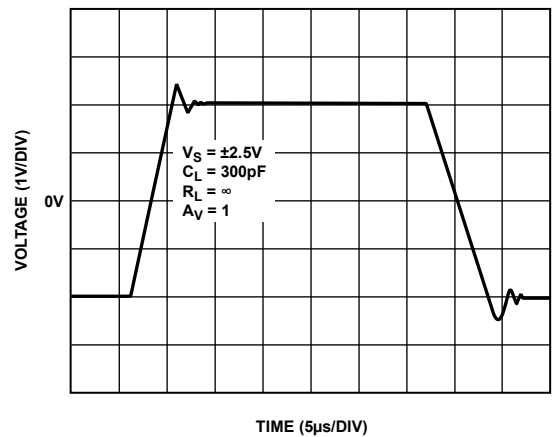


Figure 22. Large Signal Transient Response

Zero-Drift, Single-Supply, Rail-to-Rail Input/Output Operational Amplifier

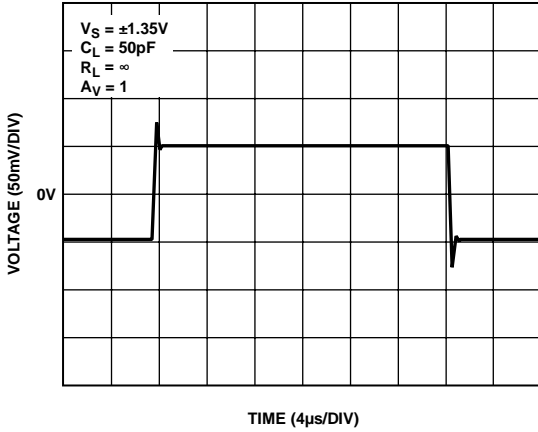


Figure 23. Small Signal Transient Response

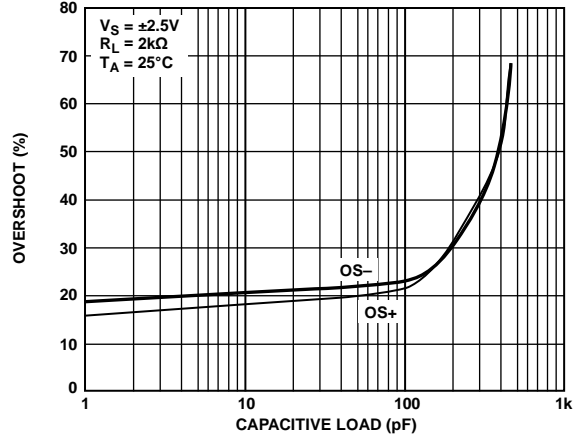


Figure 26. Small Signal Overshoot vs. Load Capacitance

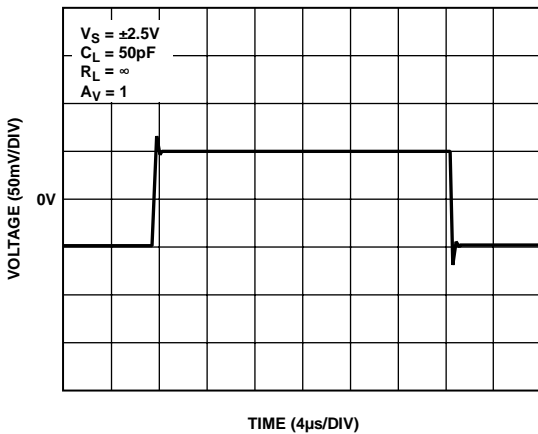


Figure 24. Small Signal Transient Response

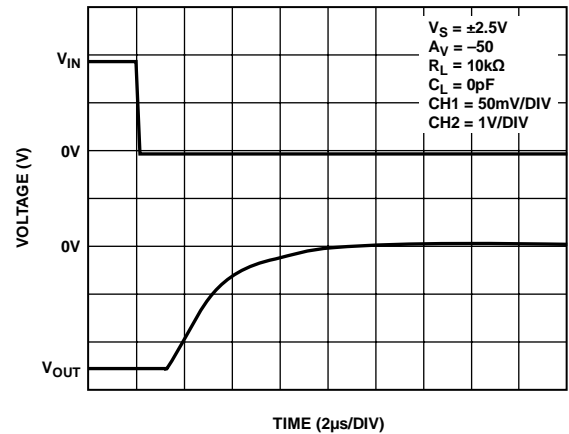


Figure 27. Positive Overvoltage Recovery

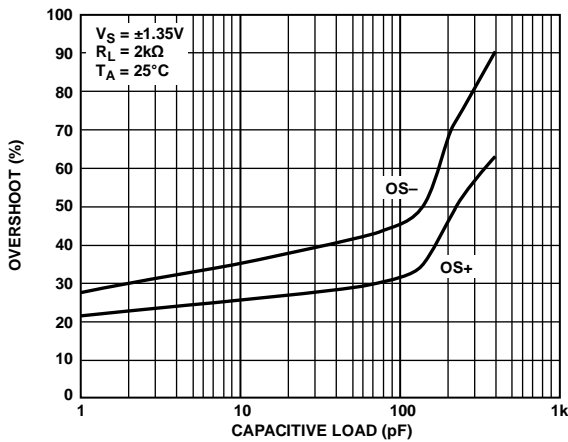


Figure 25. Small Signal Overshoot vs. Load Capacitance

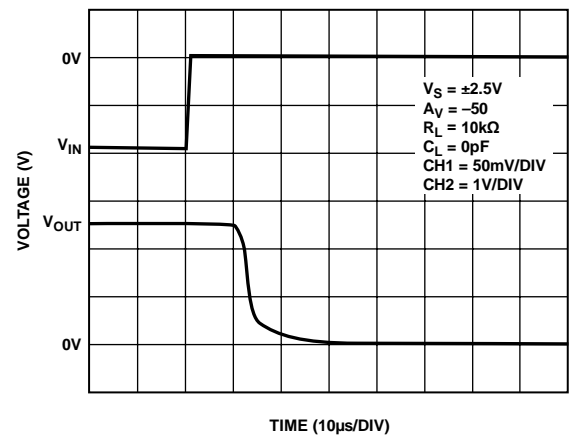


Figure 28. Negative Overvoltage Recovery

Zero-Drift, Single-Supply, Rail-to-Rail Input/Output Operational Amplifier

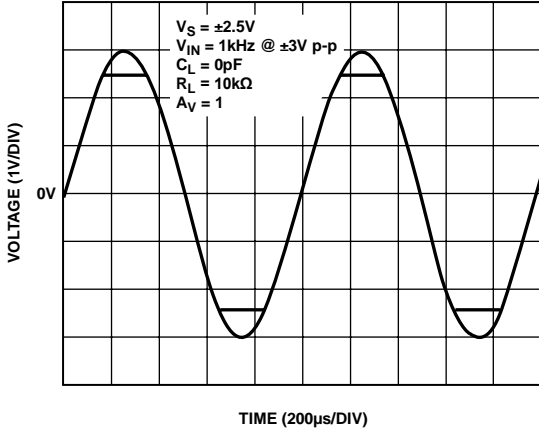


Figure 29. No Phase Reversal

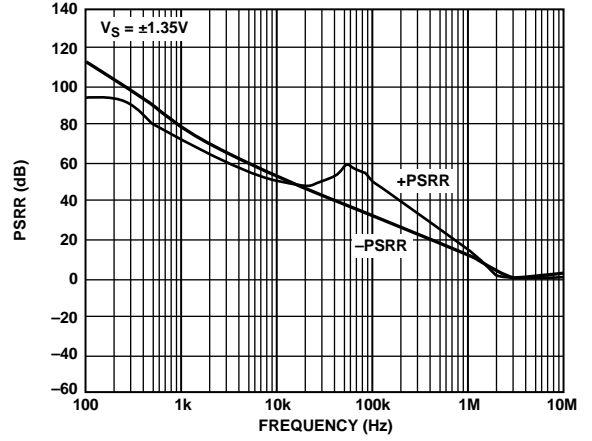


Figure 32. PSRR vs. Frequency

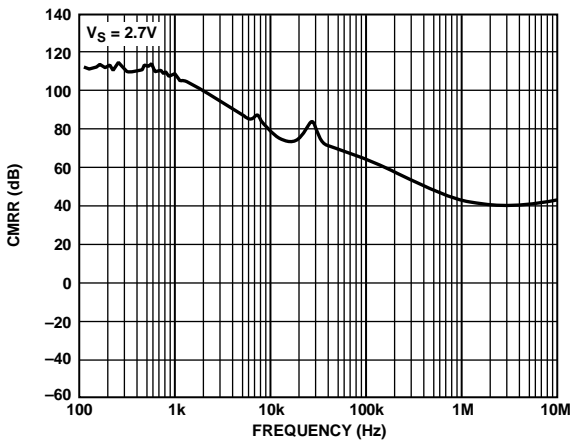


Figure 30. CMRR vs. Frequency

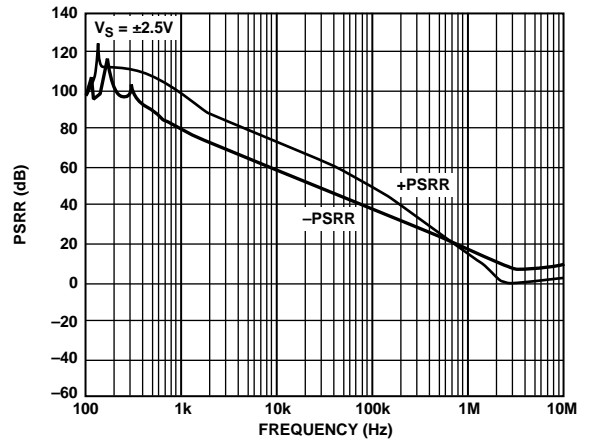


Figure 33. PSRR vs. Frequency

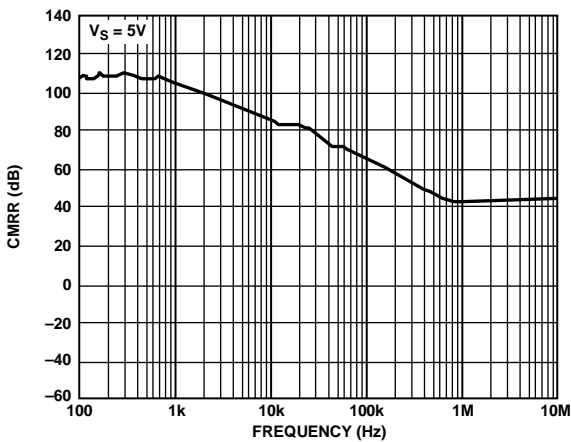


Figure 31. CMRR vs. Frequency

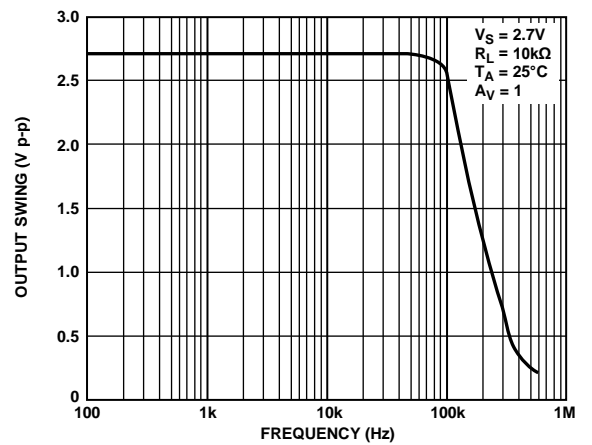


Figure 34. Maximum Output Swing vs. Frequency



Zero-Drift, Single-Supply, Rail-to-Rail Input/Output Operational Amplifier

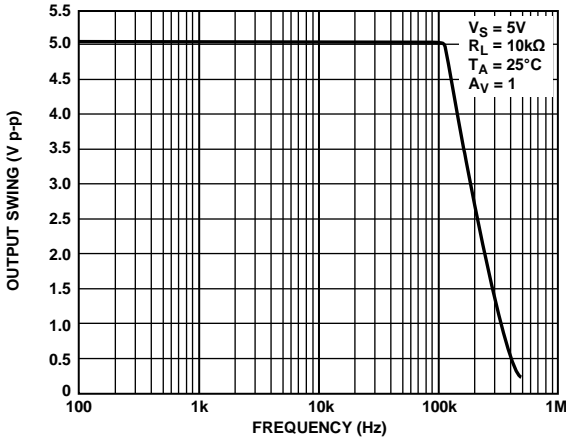


Figure 35. Maximum Output Swing vs. Frequency

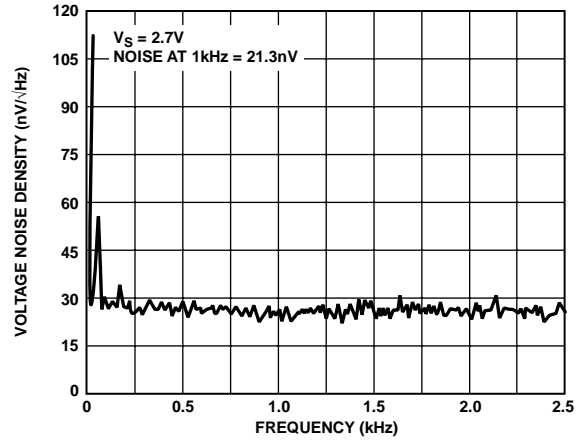


Figure 38. Voltage Noise Density at 2.7 V from 0 Hz to 2.5 kHz

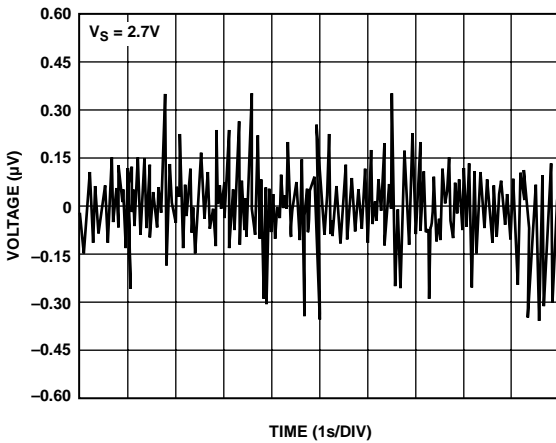


Figure 36. 0.1 Hz to 10 Hz Noise

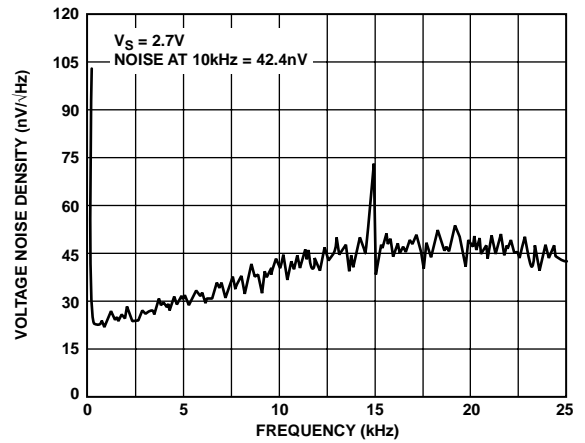


Figure 39. Voltage Noise Density at 2.7 V from 0 Hz to 25 kHz

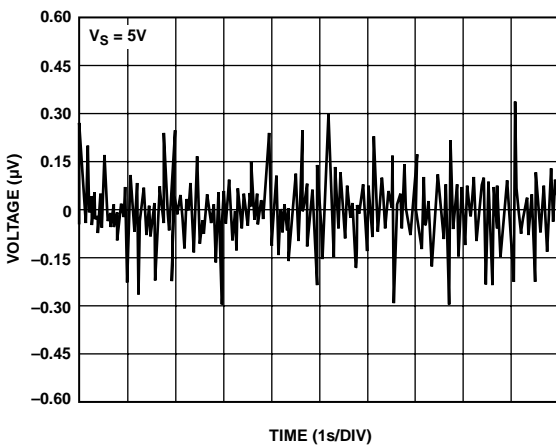


Figure 37. 0.1 Hz to 10 Hz Noise

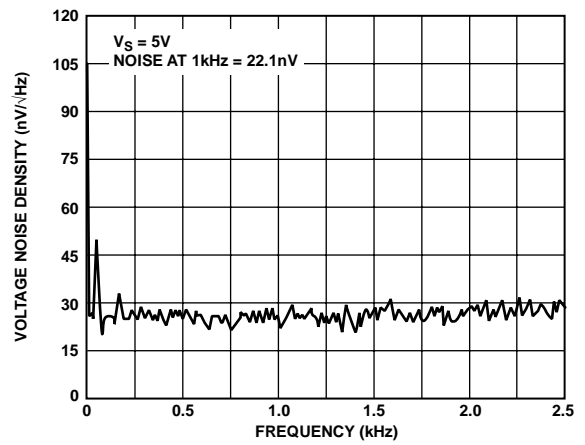


Figure 40. Voltage Noise Density at 5 V from 0 Hz to 2.5 kHz

Zero-Drift, Single-Supply, Rail-to-Rail Input/Output Operational Amplifier

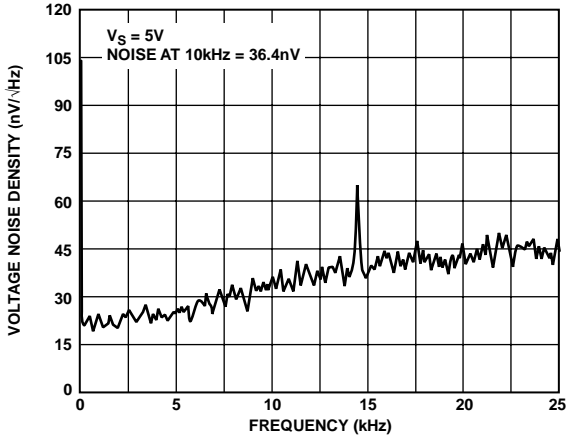


Figure 41. Voltage Noise Density at 5 V from 0 Hz to 25 kHz

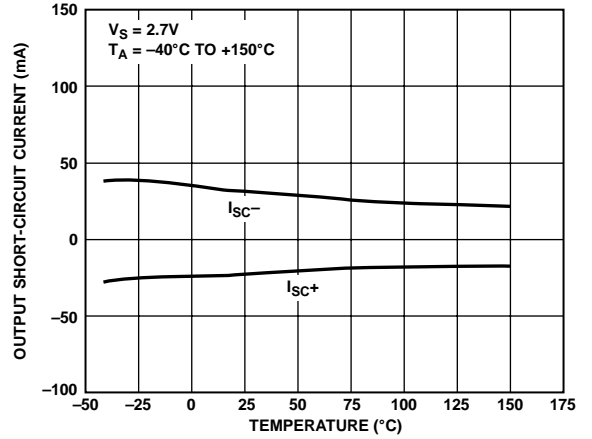


Figure 44. Output Short-Circuit Current vs. Temperature

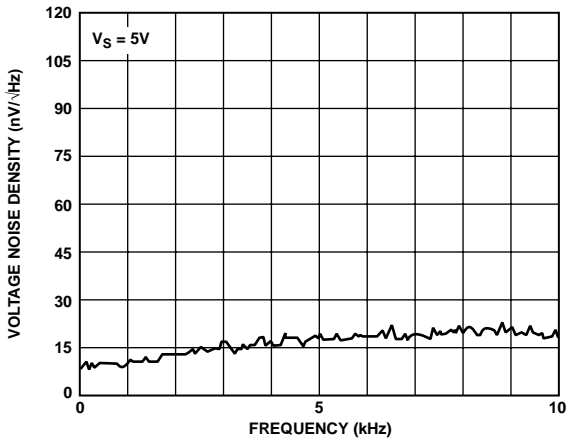


Figure 42. Voltage Noise Density at 5 V from 0 Hz to 10 kHz

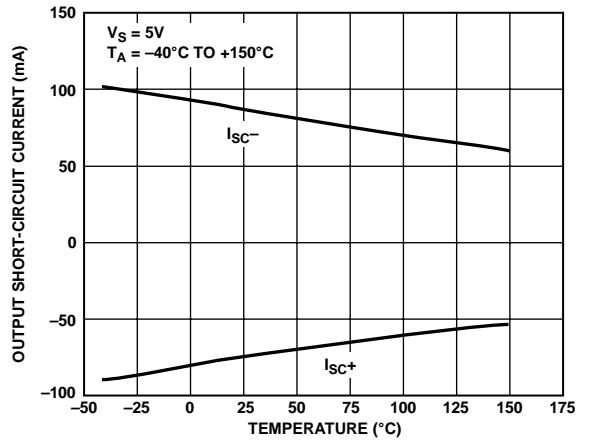


Figure 45. Output Short-Circuit Current vs. Temperature

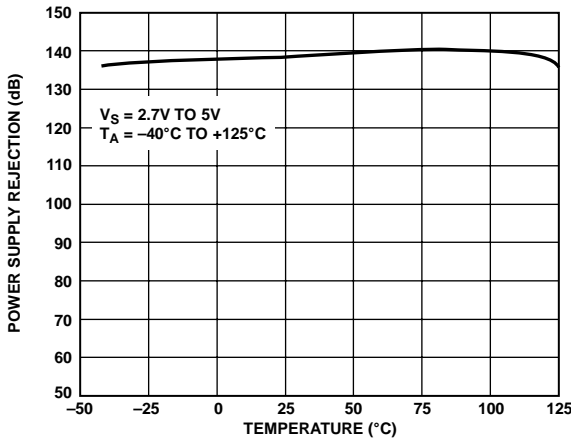


Figure 43. Power Supply Rejection vs. Temperature

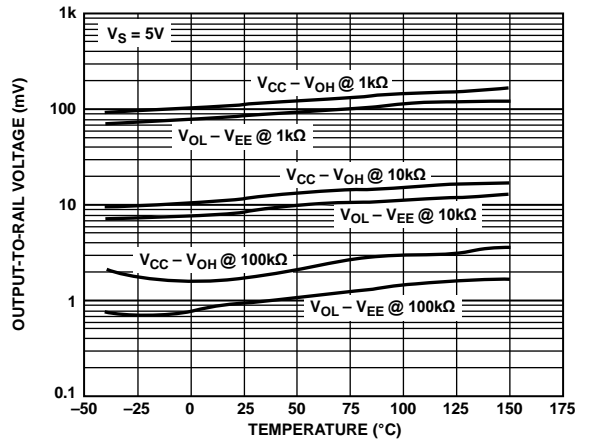


Figure 46. Output-to-Rail Voltage vs. Temperature

Zero-Drift, Single-Supply, Rail-to-Rail Input/Output Operational Amplifier

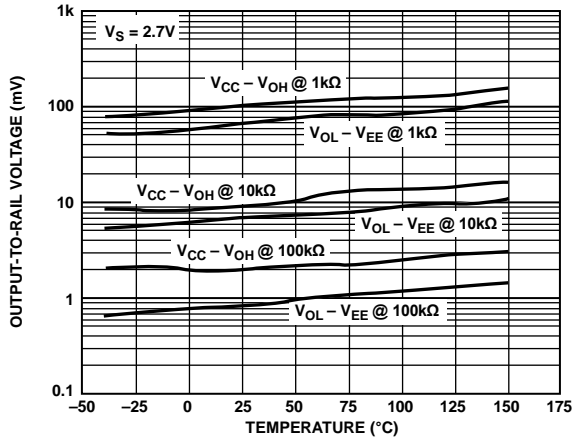


Figure 47. Output-to-Rail Voltage vs. Temperature

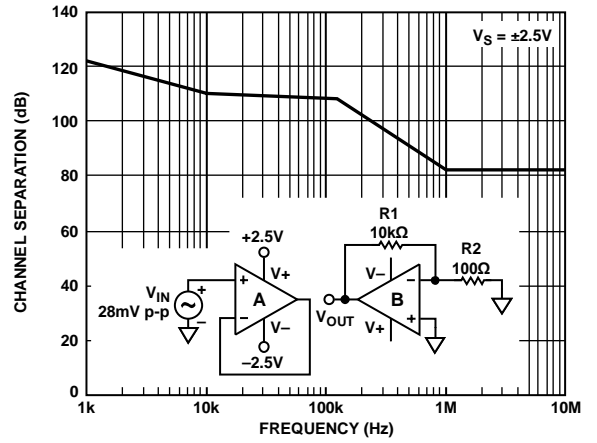


Figure 48. AD8629/AD8630 Channel Separation vs. Frequency

**PEAK-TOPEAK NOISE**

Because of the ping-pong action between auto-zeroing and chopping, the peak-to-peak noise of the AD8628/AD8629/AD8630 is much lower than the competition. Figure 50 and Figure 51 show this comparison.

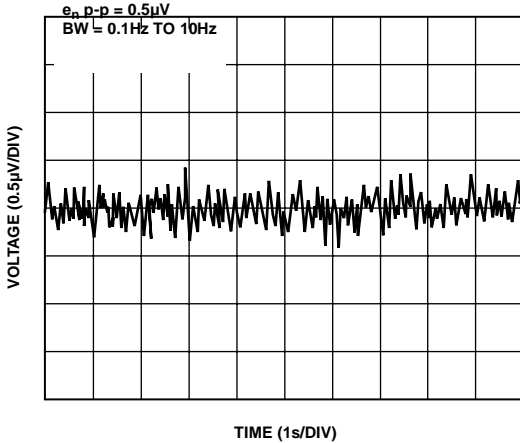


Figure 49. AD8628 Peak-to-Peak Noise

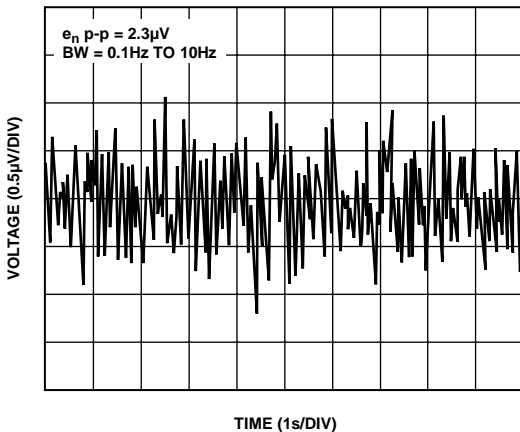


Figure 50. Competitor A Peak-to-Peak Noise

**NOISE BEHAVIOR WITH FIRST-ORDER, LOW-PASS FILTER**

The AD8628 was simulated as a low-pass filter (see Figure 53) and then configured as shown in Figure 52. The behavior of the AD8628 matches the simulated data. It was verified that noise is rolled off by first-order filtering. Figure 53 and Figure 54 show the difference between the simulated and actual transfer functions of the circuit shown in Figure 52.

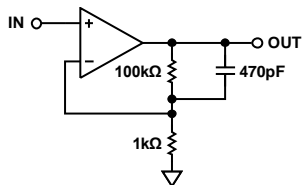


Figure 51. First-Order Low-Pass Filter Test Circuit, x101 Gain and 3 kHz Corner Frequency

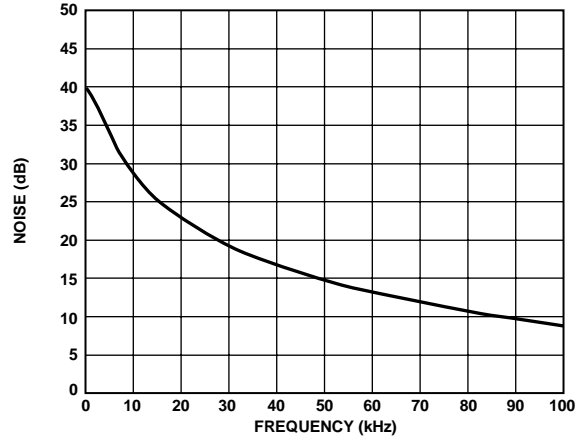


Figure 52. Simulation Transfer Function of the Test Circuit in Figure 52

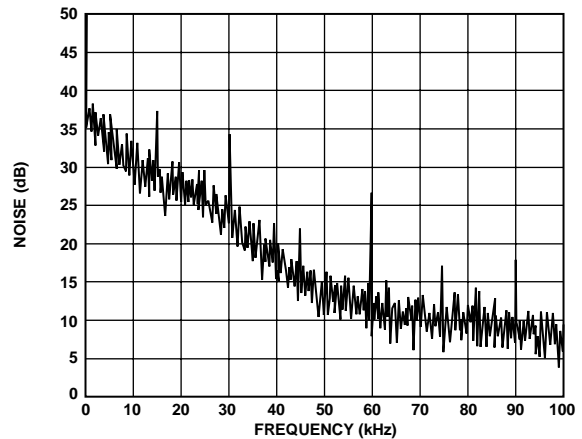


Figure 53. Actual Transfer Function of the Test Circuit in Figure 52

The measured noise spectrum of the test circuit charted in Figure 54 shows that noise between 5 kHz and 45 kHz is successfully rolled off by the first-order filter.

**TOTAL INTEGRATED INPUT-REFERRED NOISE FOR FIRST-ORDER FILTER**

For a first-order filter, the total integrated noise from the AD8628 is lower than the noise of Competitor A.

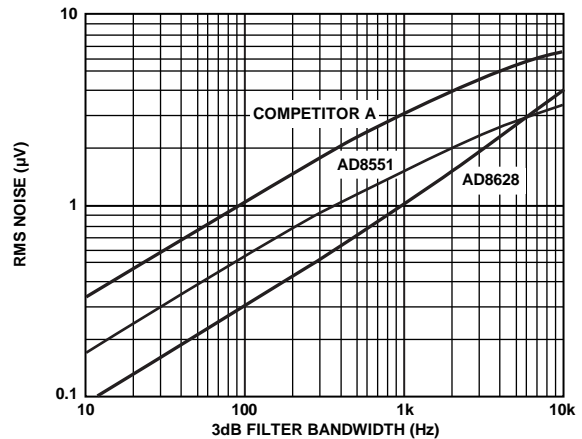


Figure 54. RMS Noise vs 3 dB Filter Bandwidth in Hz

**INPUT OVERVOLTAGE PROTECTION**

Although the AD8628/AD8629/AD8630 are rail-to-rail input amplifiers, care should be taken to ensure that the potential difference between the inputs does not exceed the supply voltage. Under normal negative feedback operating conditions, the amplifier corrects its output to ensure that the two inputs are at the same voltage. However, if either input exceeds either supply rail by more than 0.3 V, large currents begin to flow through the ESD protection diodes in the amplifier.

These diodes are connected between the inputs and each supply rail to protect the input transistors against an electrostatic discharge event, and they are normally reverse-biased. However, if the input voltage exceeds the supply voltage, these ESD diodes can become forward-biased. Without current limiting, excessive amounts of current could flow through these diodes, causing permanent damage to the device. If inputs are subject to overvoltage, appropriate series resistors should be inserted to limit the diode current to less than 5 mA maximum.

**OUTPUT PHASE REVERSAL**

Output phase reversal occurs in some amplifiers when the input common-mode voltage range is exceeded. As common-mode voltage is moved outside the common-mode range, the outputs of these amplifiers can suddenly jump in the opposite direction to the supply rail. This is the result of the differential input pair shutting down, causing a radical shifting of internal voltages that results in the erratic output behavior.

The AD8628/AD8629/AD8630 amplifiers have been carefully designed to prevent any output phase reversal, provided that both inputs are maintained within the supply voltages. If one or both inputs could exceed either supply voltage, a resistor should be placed in series with the input to limit the current to less than 5 mA. This ensures that the output does not reverse its phase.

**OVERLOAD RECOVERY TIME**

Many auto-zero amplifiers are plagued by a long overload recovery time, often in ms, due to the complicated settling behavior of the internal nulling loops after saturation of the outputs. The AD8628/AD8629/AD8630 have been designed so that internal settling occurs within two clock cycles after output saturation occurs. This results in a much shorter recovery time, less than 10 μs, when compared to other auto-zero amplifiers. The wide bandwidth of the AD8628/AD8629/AD8630 enhances performance when the parts are used to drive loads that inject transients into the outputs. This is a common situation when an amplifier is used to drive the input of switched capacitor ADCs.

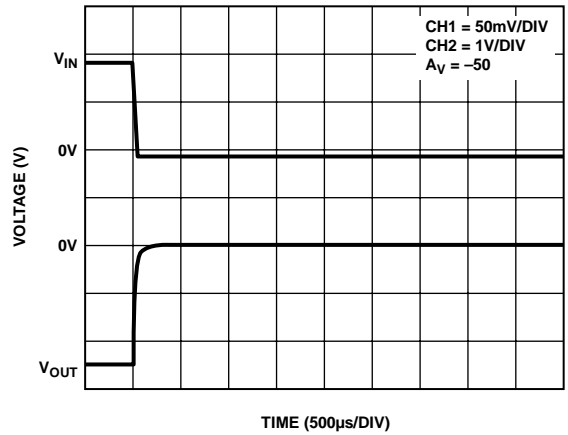


Figure 55. Positive Input Overload Recovery for the AD8628

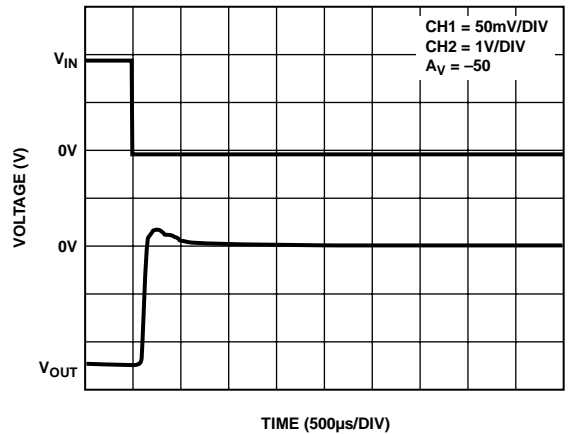


Figure 56. Positive Input Overload Recovery for Competitor A

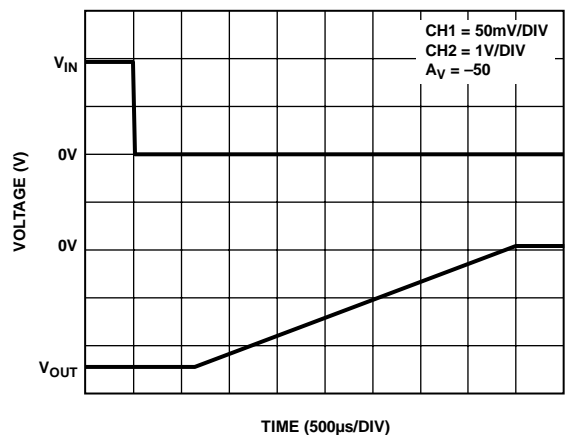


Figure 57. Positive Input Overload Recovery for Competitor B

**SENSORS**

Infrared (IR) sensors, particularly thermopiles, are increasingly being used in temperature measurement for applications as wide ranging as automotive climate control, human ear thermometers, home insulation analysis, and automotive repair diagnostics. The relatively small output signal of the sensor demands high gain with very low offset voltage and drift to avoid dc errors.

If interstage ac coupling is used, as in Figure 61, low offset and drift prevent the output of the input amplifier from drifting close to saturation. The low input bias currents generate minimal errors from the output impedance of the sensor. As with pressure sensors, the very low amplifier drift with time and temperature eliminate additional errors once the temperature measurement is calibrated. The low 1/f noise improves SNR for dc measurements taken over periods often exceeding one-fifth of a second.

Figure 61 shows a circuit that can amplify ac signals from 100  $\mu$ V to 300  $\mu$ V up to the 1 V to 3 V levels, with a gain of 10,000 for accurate analog-to-digital conversion.

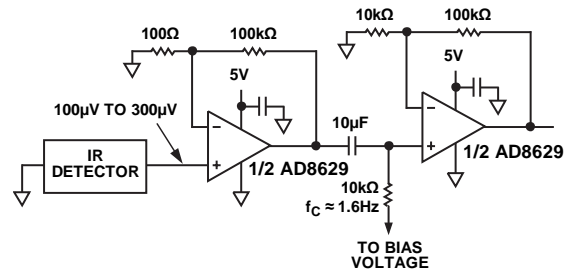


Figure 61. AD8629 Used as Preamplifier for Thermopile

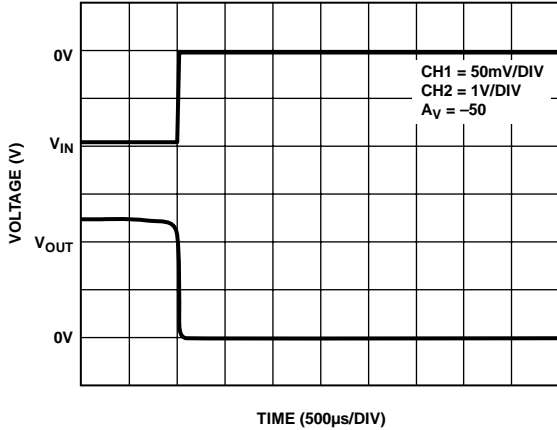


Figure 58. Negative Input Overload Recovery for the AD8628

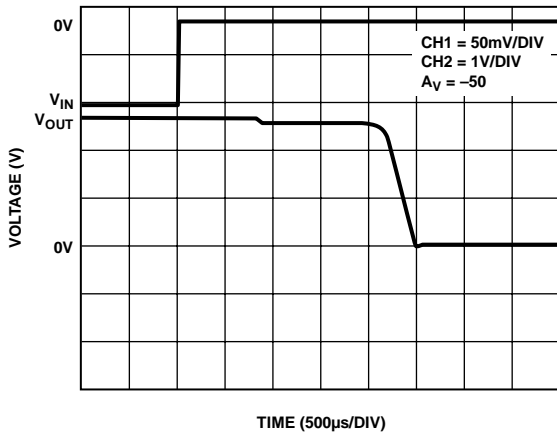


Figure 59. Negative Input Overload Recovery for Competitor A

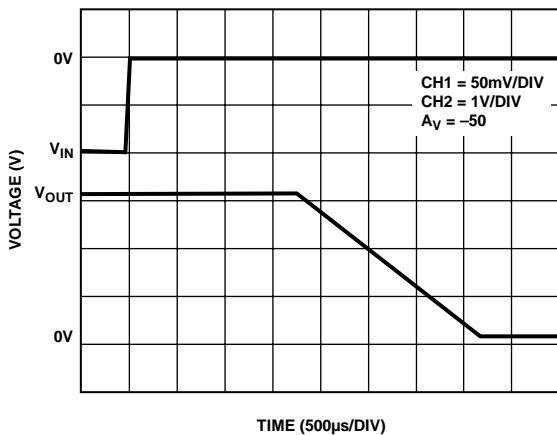
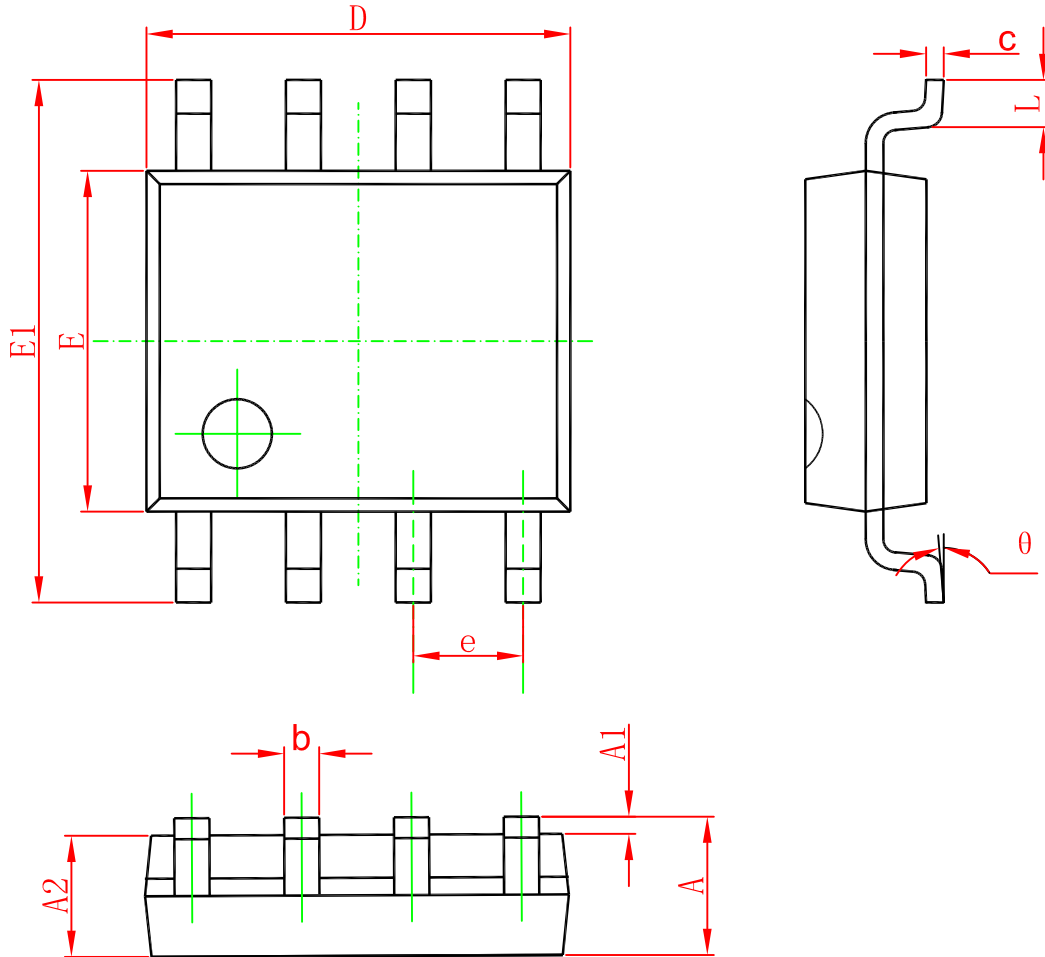


Figure 60. Negative Input Overload Recovery for Competitor B

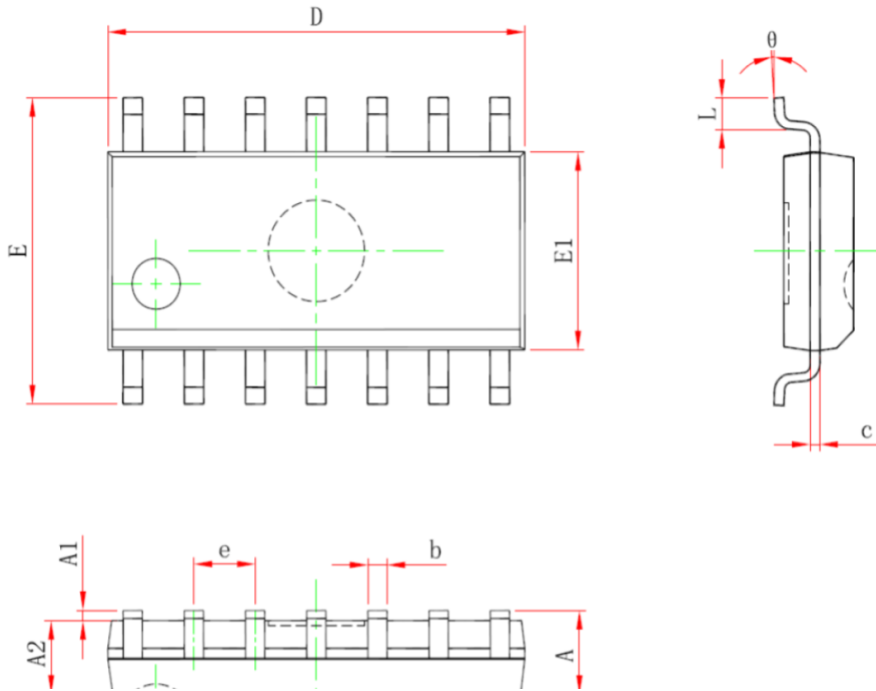
Package Mechanical

SOP-8



Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	1.350	1.750	0.053	0.069
A1	0.100	0.250	0.004	0.010
A2	1.350	1.550	0.053	0.061
b	0.330	0.510	0.013	0.020
c	0.170	0.250	0.006	0.010
D	4.700	5.100	0.185	0.200
E	3.800	4.000	0.150	0.157
E1	5.800	6.200	0.228	0.244
e	1.270(BSC)		0.050(BSC)	
L	0.400	1.270	0.016	0.050
θ	0°	8°	0°	8°

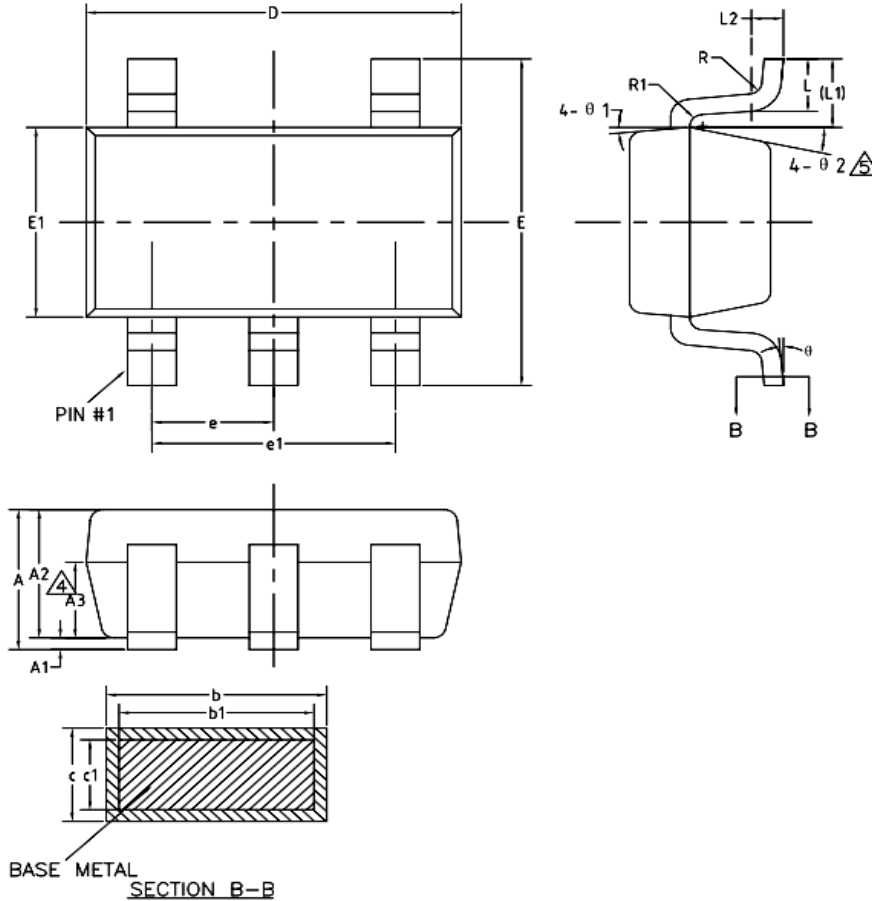
**SOP-14**



Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	---	1.750	---	0.069
A1	0.100	0.250	0.004	0.010
A2	1.250	---	0.049	---
b	0.310	0.510	0.012	0.020
c	0.100	0.250	0.004	0.010
D	8.450	8.850	0.333	0.348
E	5.800	6.200	0.228	0.244
E1	3.800	4.000	0.150	0.157
e	1.270(BSC)		0.050(BSC)	
L	0.400	1.270	0.016	0.050
θ	0°	8°	0°	8°



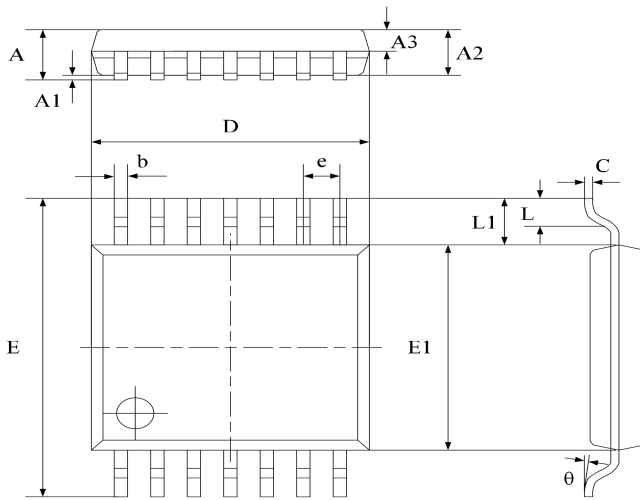
SOT23-5



COMMON DIMENSIONS  
(UNITS OF MEASURE=MILLIMETER)

SYMBOL	MIN	NOM	MAX
A	—	—	1.25
A1	0	—	0.15
A2	1.00	1.10	1.20
A3	0.60	0.65	0.70
b	0.36	—	0.50
b1	0.36	0.38	0.45
c	0.14	—	0.20
c1	0.14	0.15	0.16
D	2.826	2.926	3.026
E	2.60	2.80	3.00
E1	1.526	1.626	1.726
e	0.90	0.95	1.00
e1	1.80	1.90	2.00
L	0.35	0.45	0.60
L1	0.59REF		
L2	0.25BSC		
R	0.10	—	—
R1	0.10	—	0.25
$\theta$	0°	—	8°
$\theta 1$	3°	5°	7°
$\theta 2$	6°	—	14°

**TSSOP-14**



Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	-	1.200	-	0.0472
A1	0.050	0.150	0.002	0.006
A2	0.900	1.050	0.037	0.043
A3	0.390	0.490	0.016	0.020
b	0.200	0.290	0.008	0.012
C	0.130	0.180	0.005	0.007
D	4.860	5.060	0.198	0.207
E	6.200	6.600	0.253	0.269
E1	4.300	4.500	0.176	0.184
e	0.650 typ.		0.0256 typ.	
L1	1.000 ref.		0.0393 ref.	
L	0.450	0.750	0.018	0.031
θ	0°	8°	0°	8°

**Ordering information**

Order code	Package	Baseqty	Deliverymode	Marking
UMW AD8628ARTZ	SOT23-5	3000	Tape and reel	A0L UMWxx
UMW AD8628ARZ	SOP-8	2500	Tape and reel	AD8628 UMWxxxx
UMW AD8629ARZ	SOP-8	2500	Tape and reel	AD8629 UMWxxxx
UMW AD8630ARZ	SOP-14	2500	Tape and reel	AD8630 UMWxxxx
UMW AD8630ARUZ	TSSOP-14	4000	Tape and reel	AD8630 UMWxxxx